

STATIC AND DYNAMIC BUCKLING OF SHALLOW SPHERICAL SHELLS SUBJECTED TO AXISYMMETRIC AND NEARLY AXISYMMETRIC STEP PRESSURE LOADS USING SATANS-IIA, A MODIFIED VERSION OF SATANS-II

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THESIS

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by

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December 1976

Thesis Advisor:

Robert E. Ball

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SATANS-II

by

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Lieutenant
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ABSTRACT

A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. A comparison was made between the new buckling results and previous results obtained without the new pole routine. The comparison revealed a significant change in the buckling pressures, due solely to the change in the pole routine. The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells.

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LIST OF SYMBOLS

b	= nondimensional inplane stiffness
E	= the modulus of elasticity of the shell
H	= the rise of the spherical cap at the pole
h	= the thickness of the shell
m	= the mass density of the shell
M_s	= the meridional bending moment per unit length
n	= the Fourier index
P	= a nondimensional applied load
P_{CRIT}	= the nondimensional critical pressure
q_o	= the classical buckling pressure of a complete sphere
$q^{(n)}$	= a column matrix containing the coefficients of the n^{th} term in the series expansion of the applied load
r	= the normal distance from the axis of revolution to the surface of the cap
r_o	= the normal distance from the axis to the cap in the base plane; the maximum value of r
R_s, R_θ	= the radii of curvature in the s and θ directions, respectively
s	= the meridional distance along the surface of the shell
t	= the nondimensional time
T	= the time
T_o	= a reference time

U, V, W = the displacements in the s , θ and \mathcal{J} directions, respectively
 u, v, w = nondimensional series coefficients of U, V, W
 \bar{V} = a nondimensional measure of the volume of the shell deformation
 \bar{V}_{MAX} = the peak in the time history of the parameter \bar{V}
 $w^{(n)}$ = the displacement in the \mathcal{J} direction in the n^{th} harmonic
 δt = the nondimensional time increment
 = distance between stations
 $\epsilon^{(n)}$ = the nondimensional parameter governing the magnitude of the load applied in the asymmetric harmonics
 \mathcal{J} = the coordinate normal to the surface of the shell
 θ = the circumferential angle measured about the axis of revolution
 λ = a nondimensional geometric parameter used to describe the spherical cap
 ν = Poisson's ratio
 ξ = the normal distance from the base plane to the middle surface of the undeformed cap

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I. INTRODUCTION

In 1973 a digital computer study was presented by Ball and Burt [1] for the dynamic buckling load of clamped shallow spherical shells subjected to axisymmetric and nearly axisymmetric step-pressure loads. A static buckling analysis of the same spherical shells had been carried out in 1970 by Stilwell and Ball [2]. In these two studies the digital computer program SATANS-I [3] was used to calculate the critical buckling pressures for a large range of shell sizes. Other studies of the buckling of shallow shells have been conducted by Huang [4,5], by Stephens and Fulton [6], by Lock et al. [7], by Stricklin [8], and most recently by Akkas [9]. In Reference 1 the results from these other studies, except for those by Akkas, are compared with the results from SATANS-I for both static and dynamic buckling. In the axisymmetric static analysis the comparison with the results obtained by Huang [4] revealed that the SATANS-I results were higher than Huang's results for several shell sizes. In the dynamic, axisymmetric buckling analysis the SATANS-I results again either agreed closely with, or were somewhat higher than, the results by Huang [5], Stephens and Fulton [6], and Stricklin [8]. However, it was noted then that there was a general lack of consistent agreement among any of the sets of results. As a consequence, it appeared at that time that the axisymmetric buckling problem had not yet been totally resolved and that additional studies would be appropriate.

In the asymmetric dynamic buckling analysis of Reference 1 the few comparisons that could be made for the critical load also indicated that the SATANS-I results may be too

high. A comparison of the recent estimates for the asymmetric dynamic buckling load obtained by Akkas [9] with the SATANS-I results also reveals the SATANS-I results to be well above those of Akkas [9]. However, it should be noted that the results obtained by Akkas were from his attempt to obtain a lower bound on the critical asymmetric load. This bound on the buckling load is obtained without the execution of a complete transient response analysis on the asymmetric part of the response of the shell, as is done in SATANS-I. In Akkas' analysis (Problem 1) the transient nonlinear axisymmetric response is computed, and a determinant is examined for possible bifurcation into asymmetric motion at each time step. The minimum load at which the determinant becomes zero is defined as the lower bound of the critical load.

As a consequence of the generally high buckling loads predicted by SATANS-I, a re-examination of the static and dynamic buckling of the shallow spherical shell was made in an attempt to determine the possible cause, or causes, of the high buckling loads. In our search we discovered that a modification of the manner in which the pole conditions are numerically approximated significantly lowered the buckling loads to values that are now in good agreement with the other results. The new procedure for handling the pole condition is given in section III of this thesis. The new buckling results are given in section V.

In addition to the pole condition modifications and the new buckling results the author has also made another significant change to the SATANS family of codes. In particular, the SATANS-II program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution, developed by Ryan [10] in 1972 to handle more complex and larger problems, was modified to make the computer memory requirement a variable quantity. This

quantity is specified by the user to fit the particular problem being run. It eliminates the large core requirement of SATANS-II for small problems and allows for much larger problems to be solved than could be solved by SATANS-II. The new program with the pole condition and memory modifications will hereafter be called SATANS-IIA. It is described in section II.

II. DESCRIPTION OF SATANS-IIA

SATANS-II was developed by Ryan [10] from SATANS-I and incorporated the full trigonometric expansion of the applied load and solution vector, and introduced the handling of imperfections into the code. These modifications allow the analysis of shells under totally arbitrary loads, as well as imperfection studies on actual shells with measured imperfections [11]. Unfortunately, the original deck of cards for SATANS-II was destroyed. Professor Johann Arbocz of CALTECH had a listing of SATANS-II and punched a deck of cards with the changes to SATANS-I given in that listing. A copy of this deck was sent to Professor Ball. These cards have been added by the author to the original SATANS-I described by Ryan [10] and a complete version of SATANS-II has been reconstructed. SATANS-IIA is a modification by the author of the reconstructed SATANS-II program. A listing of SATANS-IIA can be found in Appendix A. The listing contains an example problem for the dynamic analysis of a clamped, truncated cone subjected to an impulsive loading which is uniform along the meridian and varies in a cosine distribution over one-half of the circumference. This problem is a sample problem suggested by the Lockheed Missiles and Space Corp. [12]. A condensed version of the output from the example problem is given in Appendix B. Input data preparation for SATANS-IIA can be found in Appendix C. The basic users manual, which includes preparation of input subroutines and the theory of the program, is contained in Reference 3, which can be obtained through COSMIC (M70-10098, LAR-10736), or ASIAC [13]. A users manual which includes preparation and handling of imperfection data within the SATANS programs can be found in

Ref. [10]. The above information, along with the following discussion, will inform the user on the capabilities and proper use of SATANS-IIA.

The modification of the SATANS-II program to make its core requirement variable was accomplished by putting in a single dimension statement at the beginning of the program, with subsequent dimensioning within the subroutines to only the first element of the vector or matrix. This is a convenient feature of the FORTRAN-IV language in which the program is written. The actual vector and matrix sizes are transmitted to the subroutines by an individual parameter list. Construction of the initial dimension statement and core request size is as follows:

The basic size of the program on the IBM-360/67 Digital Computer, without the initial dimension statement, is 272,000 bytes. This figure includes approximately 19,000 bytes of buffer space required for execution. Within the main dimension statement are fifteen variables. However, only three parameters are needed to specify the sizes of these fifteen variables.

Let a = The number of stations along the meridian of the shell times the number of harmonics considered.

Let b = a , plus two fictitious stations times the number

of harmonics considered.

Let c = The number of harmonics considered.

The main dimension statement would then be constructed as,

```
DIMENSION P(4,4,a), DEE(4,4,a), DST(4,4,a), X(4,a),  
           PHIXB(a), PHITB(a), Z(4,b), ZO(4,b),  
           Z2(4,b), Z3(4,b), ZDOT(4,b), IS(99,c),  
           JS(99,c), ID(99,c), JD(99,c)
```


The 99's above limit the user to 99 harmonics in any one run and an unlimited number of meridional stations. The core requirement for the general case would be,

$$272,000 + 216a + 80b + 1584c = \text{bytes of core required.}$$

For a sample calculation of the core requirements consider the example of a spherical cap with 40 stations along the meridian, and an asymmetric analysis with two harmonics. Therefore,

$$a = 40(\text{stations}) \times 2(\text{harmonics}) = 80$$

$$b = 80 + 2 \times 2(\text{harmonics}) = 84$$

$$c = 2(\text{harmonics})$$

Thus, for the variables P, DEE, DST,

$$3 \times (4 \times 4 \times 80) = 3840 \text{ (words)} \times 4 = 15,360 \text{ bytes}$$

for the variable X,

$$4 \times (80) = 320 \text{ (words)} \times 4 = 1280 \text{ bytes}$$

for the variables PHIXB, PHITB,

$$2 \times (80) = 160 \text{ (words)} \times 4 = 640 \text{ bytes}$$

for the variables Z, Z0, Z2, Z3, ZDOT,

$$5 \times (4 \times 84) = 1680 \text{ (words)} \times 4 = 6720 \text{ bytes}$$

lastly, for the variables ID, JD, IS, JS,

$$4 \times (99 \times 2) = 792 \text{ (words)} \times 4 = 3168 \text{ bytes}$$

Therefore, the total size of the main dimension statement would be 27,168 bytes. This figure would be rounded up to the nearest even thousand bytes, i.e. 28,000 bytes. Finally, the core requirement for this example problem would be

$$272,000 + 28,000 = 300,000 \text{ bytes.}$$

III. IMPROVED POLE ROUTINE

The SATANS code is based upon Sander's geometrically nonlinear equations under the conditions of small strains and moderately small rotations. The formulation is in four second order nonlinear partial differential equations in terms of U , V , W , and M_s , where U , V , and W are the meridional, circumferential and normal displacements respectively, and M_s is the meridional bending moment. The nonlinear partial differential equations in the coordinates s , θ , and t are reduced to uncoupled sets of linear differential equations in s and t by expanding the variables in trigonometric series in the circumferential coordinate θ , and treating the nonlinear terms as pseudo loads. The first and second derivatives in the meridional coordinate s are replaced by the conventional central finite difference approximations, i.e.

$$\{z\}'_i = 1/2\Delta (\{z\}_{i+1} - \{z\}_{i-1}) \quad (1)$$

and

$$\{z\}''_i = 1/\Delta^2 (\{z\}_{i+1} - 2\{z\}_i + \{z\}_{i-1}) \quad (2)$$

where $\{z\}_i$ is the vector of U , V , W , and M_s at the i^{th} station, Δ is the uniform dimension between stations, and primes denote partial derivatives with respect to s . Applying these approximations to the governing set of domain

equations leads to

$$[C]_i \{z\}_{i-1} + [B]_i \{z\}_i + [A]_i \{z\}_{i+1} = \{g\}_i \quad (3)$$

When the shell does not have a pole, fictitious stations one increment off of the shell are introduced at each end. Both the governing domain equations and the boundary conditions are applied at the two boundary points. Thus, all finite difference approximations to the derivatives, including those of the boundary conditions, are of order

Δ^2 . However, prior to the development of SATANS-IIA, the treatment of the conditions to be applied at a pole at either end of a shell was handled by a simple Euler forward or backward difference approximation to the first derivative, with truncation error of order Δ . For example, for a pole at $s=0$, where $i=1$, the first derivative at the pole was approximated with

$$\{z\}'_1 = 1/\Delta (\{z\}_2 - \{z\}_1). \quad (4)$$

At the time this procedure for handling the pole conditions was developed (1967) it was thought that this would not significantly alter the solution. However, it has since been discovered that such is not the case.

For the new pole routine, an expanded forward difference approximation of order Δ^2 is used at $s=0$ which takes into account the two stations after the pole, instead of just one station after the pole as in the Euler scheme. This approximation is

$$\{z\}'_1 = 1/2\Delta (-3\{z\}_1 + 4\{z\}_2 - \{z\}_3). \quad (5)$$

The conditions to be imposed upon the dependent variables at a pole are derived in Reference 14. They are :

$$\text{For } N=0, \quad u_1 = v_1 = w'_1 = m'_s = 0.$$

Applying equation (5), these conditions can be put into the matrix form

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -3 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

where the above 3 matrices are DL, DG, and DF within the SATANS programs.

$$\text{For } N=1, \quad u_1 \pm v_1 = u'_s = w = m_s = 0,$$

where the plus sign applies at an initial pole, and the minus sign at a final pole. The matrix form for these conditions is

$$\begin{bmatrix} -3 & 0 & 0 & 0 \\ 1 \pm 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N=2, \quad u = v = w = m'_s = 0$$

the matrix form is

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N > 2, \quad u = v = w = m_s = 0$$

and DL= identity matrix, DG= DF= null matrices.

The solution procedure in SATANS is an elimination scheme and starts with

$$\{z\}_1 = - [P]_1 \{z\}_2 + \{x\}_1, \quad (6)$$

where the values in $[P]_1$ based upon the Euler approximation are defined in Reference 14. The higher order approximation defines a new $[P]_1$. This new $[P]_1$ is obtained by simultaneously solving the pole conditions

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] \{z\}_3 = \{0\}, \quad (7)$$

and the domain equation at station 2 next to the pole

$$[C]_2 \{z\}_1 + [B]_2 \{z\}_2 + [A]_2 \{z\}_3 = \{g\}_2, \quad (8)$$

to eliminate $\{z\}_3$. Thus,

$$\{z\}_3 = [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2). \quad (9)$$

Substituting equation (9) into equation (7) gives

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2) = 0. \quad (10)$$

Combining like coefficients of the $\{z\}$ vector leads to

$$([DL] - [DF] [A]_2^{-1} [C]_2) \{z\}_1 + ([DG] - [DF] [A]_2^{-1} [B]_2) \{z\}_2 = - [DF] [A]_2^{-1} \{g\}_2. \quad (11)$$

Finally, solving for $\{z\}_1$ yields

$$\begin{aligned} \{z\}_1 &= - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2] \{z\}_2 \\ &+ [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2. \end{aligned} \quad (12)$$

Thus, $[P]_1 = - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2]$ and $\{x\}_1 = [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2$. The new $[P]_1$ matrix has been placed into the "PMATRIX" subroutine of SATANS-IIA and the new $\{x\}_1$ vector has been placed in the "FORCE" subroutine.

A listing of the pole routine may be found in Appendix D. To incorporate this new routine into a SATANS-I or-II program, first proceed to the "PMATRIX" subroutine and remove the fifteen cards that are between, but not including, "IF(NN.GT.2) GO TO 90" and "11 CONTINUE". These cards are located after statement number "14" and just before statement number "11". Replace the cards removed by the ones listed in Appendix D which read from "C IN PMATRIX" to "90 M3=MN". Then proceed to the "FORCE" subroutine and remove statement number "10". Replace statement number "10" with the nine cards listed in Appendix D which read from "C IN FORCE" to "DO 11 I= 1,4". Also place "COMMON /IBL5/IBCINL, IBCFNL" into the common area of the "FORCE" subroutine.

This completes the implementation of the new pole routine into either SATANS-I or II.

IV. PROBLEM DESCRIPTION

The geometry of the shallow spherical shell used in this study is identical to that used in Reference 1. Briefly, the shallow shell can be specified by the non-dimensional parameter λ , where

$$\lambda = 2[3(1 - \nu^2)]^{1/4} (H/h)^{1/2}. \quad (1)$$

H is the rise of the shell, h is the thickness, and ν is Poisson's ratio. The mass density of the shell is m . All shells analyzed had the following dimensions;

Radii of Curvature	$R = R_s = 250$ inches
Thickness	$h = 0.25$ inches
Modulus of Elasticity	$E = 30,000,000$ psi
Poisson's Ratio	$\nu = 0.3$

All buckling pressures obtained will be listed as a percent of the classical buckling pressure of a complete sphere, q_0 , where

$$q_0 = [2E(h/R_s)^2] / [3(1 - \nu^2)]^{1/2} \quad (2)$$

Forty stations were used over the meridian. The nondimensional time increment δt , where

$$t = T / (R_s^2 m / E)^{1/2}, \quad (3)$$

was taken as 0.05 for 3000 time steps, which is a total nondimensional time of 150. In addition, the axisymmetric analysis was repeated with a larger time step of $\delta t = 0.2$ for a total time of 600. In this study m was selected such that t is equal to T . The necessity for the long response time is explained in Reference 6.

In the axisymmetric analysis only the $N = 0$ harmonic is considered. However, in the asymmetric analysis a second harmonic is excited by applying an incremental load in that harmonic. In addition, analyses of the shells $\lambda = 6, 7.5$, and 11 were made using five harmonics. The step pressure load for the axisymmetric harmonic is

$$\{q^{(0)}\} = P q_0 \{1\}, \quad (4)$$

and the step pressure load for the asymmetric second harmonic is

$$\{q^{(n)}\} = P q_0 \xi^{(n)} \{1\}, \quad (5)$$

where $n > 0$, and $\xi^{(n)}$ is taken as 0.0001. The value taken for the second harmonic in the asymmetric analysis was the same as the critical harmonic for the static buckling analysis presented by Stilwell and Ball [2]. When there was an uncertainty as to which was the critical static harmonic the two harmonics in question were both tested. Run times using SATANS-IIA with a two-harmonic analysis for 3000 time steps and 40 stations on the meridian took an average of 28 minutes on the IBM 360/67.

The parameter used to determine the minimum load at which dynamic buckling occurs is the peak value of \bar{V} , called

\bar{V}_{MAX} , where \bar{V} is defined as

$$\bar{V} = \int_0^{r_0} r w^{(0)} dr / \int_0^{r_0} r \xi dr \quad (6)$$

r is the normal distance from the axis to the shell, r_0 is the maximum value of r , $w^{(0)}$ is the normal displacement of the axisymmetric response and ξ is the vertical distance from the base plane to the undeformed shell. The \bar{V} is a measure of the volume of the shell deformation. The Fortran statements computing \bar{V} and \bar{V}_{MAX} are given in Appendix E.

When working a problem that requires these calculations the nineteen cards are inserted directly into the "DYNAMIC" subroutine right after the "IF" statement that calls the "OUTPUT" subroutine.

For convenience, the response in each asymmetric harmonic is also measured using equation (6), with $w^{(0)}$ replaced with $w^{(n)}$. The parameter \bar{V} for the asymmetric harmonics does not represent a volume of deformation as it does for the axisymmetric harmonic. It can, however, be used to indicate the relative excitation of the asymmetric harmonics.

The buckling criterion for both the axisymmetric and the asymmetric dynamic buckling analysis defines the critical load as that load P where a very small increase in P causes a very large increase in \bar{V}_{MAX} . This is the same criterion

as that used in Ref. [1].

V. RESULTS AND DISCUSSION

A. STATIC AXISYMMETRIC BUCKLING ANALYSIS

Table I presents the new results from the static axisymmetric buckling analyses for $\lambda = 4$ through 13 using the new pole routine. The two upper curves in Figure 1 present a comparison of the new results obtained by SATANS-IIA with those obtained by Stilwell and Ball [2] using the SATANS-I program. As can be seen in this figure, fairly significant changes in the buckling load occurred in the neighborhood of $\lambda = 4, 5$, and 9; and somewhat smaller differences occurred in the region $\lambda = 10$ through 13. The upper data points in Figure 2 present the comparison of the new results from SATANS-IIA with those obtained by Huang [4]. This comparison shows a very good agreement between the two sets of results, except for the largest values of λ . The new results have eliminated the differences that existed between the SATANS-I results and Huang's results.

B. DYNAMIC AXISYMMETRIC BUCKLING ANALYSIS

Figure 3 presents the new results for the peak value of \bar{V}_{MAX} versus P for the various values of λ tested. Table II presents all of the new results for the dynamic axisymmetric buckling load. These loads are selected from figures constructed just like Figure 3. In every case,

except for $\lambda = 4$, a value of P slightly above the P_{CRIT} value caused a \bar{V}_{MAX} indicative of buckling, as well as a nonconvergence of the iterative solution procedure.

The lower two curves of Figure 1 present a comparison versus λ of the new axisymmetric dynamic buckling results with the previous buckling results obtained by Ball and Burt [1]. In every case the new critical pressure is lower than the critical pressure obtained using the Euler approximation at the pole.

The lower data points of Figure 2 present a comparison of the new results with those obtained by Huang [5], by Stephens and Fulton [6], and by Stricklin [8]. Just as in the case of the static axisymmetric buckling analysis, the new results compare much more favorably with the other results than did the results of Reference 1. It's interesting to note that the new results now tend to be slightly lower than the other results, whereas the results of Reference 1 were higher for almost all values of λ .

C. DYNAMIC ASYMMETRIC BUCKLING ANALYSIS

Table III presents the new results for the critical pressures obtained from the dynamic asymmetric analysis. The second harmonics, or critical static harmonics, used in the analyses are also presented in Table III. A comparison of the critical pressures from the asymmetric analyses, Table III, with the critical pressures from the axisymmetric analyses, Table II, reveals that only the shell $\lambda = 6$ buckled at a load below the axisymmetric buckling load. For the shell $\lambda = 7$ the critical buckling load was slightly

larger when asymmetric motion was considered. In all other cases the buckling was not influenced by the presence of the second harmonic. These new buckling results and those by Ball and Burt [2] are plotted in Figure 4. The new results can be seen to be significantly different from the SATANS-I results, where the asymmetric buckling loads were lower than the axisymmetric loads for five out of the ten values of tested.

Except for $\lambda = 6$ and 7, the relationship between \bar{V}_{MAX} and P for the N= 0 harmonic, in the two-harmonic analyses, was found to be essentially identical to the relationship found in the axisymmetric buckling analysis shown in Figure 3. Table IV A presents the \bar{V}_{MAX} versus P data for both the N= 0 harmonic and the second harmonic, for all values of λ tested, except for $\lambda = 6$. Note that, except for $\lambda = 7$ and 11, \bar{V}_{MAX} for the asymmetric harmonic is generally very small, even when the \bar{V}_{MAX} for the N= 0 harmonic indicates that the shell has buckled. Thus, except for the shells $\lambda = 6$ and 7, the presence of the asymmetric motion does not influence the axisymmetric motion, and except for the shells $\lambda = 6, 7$ and 11 the asymmetric motion is very small prior to buckling in the axisymmetric harmonic.

A more detailed analysis of the shell $\lambda = 6$ has been conducted since it was the only shell that revealed any significant axisymmetric sensitivity to asymmetric motion. This shell was studied using two two-harmonic analyses (N= 0, 1 and N= 0, 2) and a five-harmonic analysis (N= 0, 1, 2, 3, and 4). Figure 5 and Tables IV B and IV C contain values of \bar{V}_{MAX} versus P for both of the asymmetric harmonics, N= 1

and $N = 2$, in the two two-harmonic analyses, as well as the values of \bar{V}_{MAX} for the axisymmetric harmonic, $N = 0$. Figure 6 and Table IV D present the values of \bar{V}_{MAX} versus P for the $N = 0, 1, 2, 3$, and 4 harmonics from the five-harmonic study. A comparison of the critical buckling load predicted from the results of the two two-harmonic analyses in Figure 5 with the critical load from the five-harmonic analysis obtained from Figure 6 shows that the presence of the additional harmonics results in the shell buckling at a slightly lower load (0.50), with significant motion in the $N = 1$ harmonic instead of the $N = 2$ harmonic (see the nonconverged solution at $P = 0.51$), which is the critical harmonic for static asymmetric buckling. Studies using five harmonics have also been conducted for $\lambda = 7.5$ and $\lambda = 11$. As can be seen in Table IV D the critical harmonic for $\lambda = 7.5$ remained $N = 3$; however, significant motion occurred in that harmonic at $P = .41$ and $.44$. In the case of $\lambda = 11$, relatively large asymmetric motion occurred in the asymmetric mode of $N = 5$ vice 6 at a value of $P = .46$.

The comparison of the new results for the critical pressure for dynamic asymmetric buckling with those obtained analytically by Stricklin [8], by Akkas [9], and experimentally by Lock et al [7] is illustrated in Figure 7. The comparison reveals an agreement with Stricklin in every case, in general a higher value of P_{CRIT} than those obtained by Akkas, and most importantly a very good agreement with Lock's experimental results.

When making the comparison between the new results and those obtained by Akkas, it is necessary to look at the differences in the problem solution parameters used in the two studies. For example, buckling results obtained from SATANS-IIA using the same time increment as used by Akkas,

$\delta t = .2$ for 3000 time steps, were significantly higher than those using the time step of $\delta t = .05$ for many values of λ . Furthermore, the new results had, in some cases, instances of buckling occurring as far out in time as 130. Akkas, to shorten computer run times, observed the cap only for a time of less than 5. Furthermore, only the harmonics $N = 1$ or 2 or 3 were studied by Akkas for shells $\lambda = 5$ through 12. If the critical harmonic is not studied, the predicted load will be too high. Thus, it appears that Akkas' lower bound loads may not be true lower bounds.

Two additional features of the shell response should be noted. First, shells $\lambda = 6, 7.5$, and 11 exhibited a non-buckled response in the axisymmetric harmonic to a load larger than the defined critical buckling load. This can be seen in Tables IV A and IV C. Second, and most importantly, the buckling load proposed by Ball and Burt [1], and used here, defines buckling to occur when the \bar{V}_{MAX} in the axisymmetric harmonic undergoes a large change due to a small change in P . Another criterion for dynamic buckling in the asymmetric analysis discussed in Reference 1 is to define the buckling load as that threshold load that initiates significant growth in the asymmetric harmonic. Re-examination of the \bar{V}_{MAX} versus P data in Table IV A through D reveals that shells $\lambda = 6, 7$, and 11 exhibited relatively large asymmetric motion at loads smaller than the defined buckling load when compared with other \bar{V}_{MAX} values for those shells, even though the numbers themselves were small when compared with the axisymmetric harmonic. Shells $\lambda = 7.5$ and 12 appear to be borderline cases. If the alternate criterion for buckling is used, the critical buckling loads for shells $\lambda = 6, 7$, and 11 become 0.47, 0.45, and 0.45, respectively. The shells $\lambda = 7.5$ and 12 could have buckling

loads as low as 0.40 and 0.44, respectively. These values are more conservative than the definition based upon axisymmetric response. These five shells are the same five shells that exhibited an asymmetric buckling load lower than the axisymmetric buckling load in Reference 1.

VI. SUMMARY AND CONCLUSIONS

A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program, called SATANS-IIA, was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. The cap sizes ranged from $\lambda = 4$ to 13 including $\lambda = 7.5$. A comparison was made between the new buckling results with the improved pole handling routine and the results that did not have the new pole routine. The comparison revealed a significant change in buckling pressures, due solely to the change from an order Δ finite difference approximation of the first derivatives at the pole to an approximation of order Δ^2 . These new critical pressures are in very good agreement with the results from other studies of the same spherical shells. This good agreement with other results, which came about as a result of the modification of the pole handling routine, is a strong indication that the manner in which the pole condition is handled is vital to the accuracy of the solutions obtained.

In the asymmetric analysis, two harmonics were included for most of the shells; the axisymmetric harmonic and one asymmetric harmonic. Five-harmonic analyses were conducted for three of the shells. Two buckling criteria for the

asymmetric analysis were considered. One defined buckling as that threshold load that caused a large increase in a deformation parameter, \bar{V}_{MAX} , in the axisymmetric harmonic.

The other, more conservative than the first, defined buckling as that threshold load that caused a large increase in the \bar{V}_{MAX} value for the asymmetric harmonic. Both values have been presented.

The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells. The effect of realistic imperfections remains to be determined.

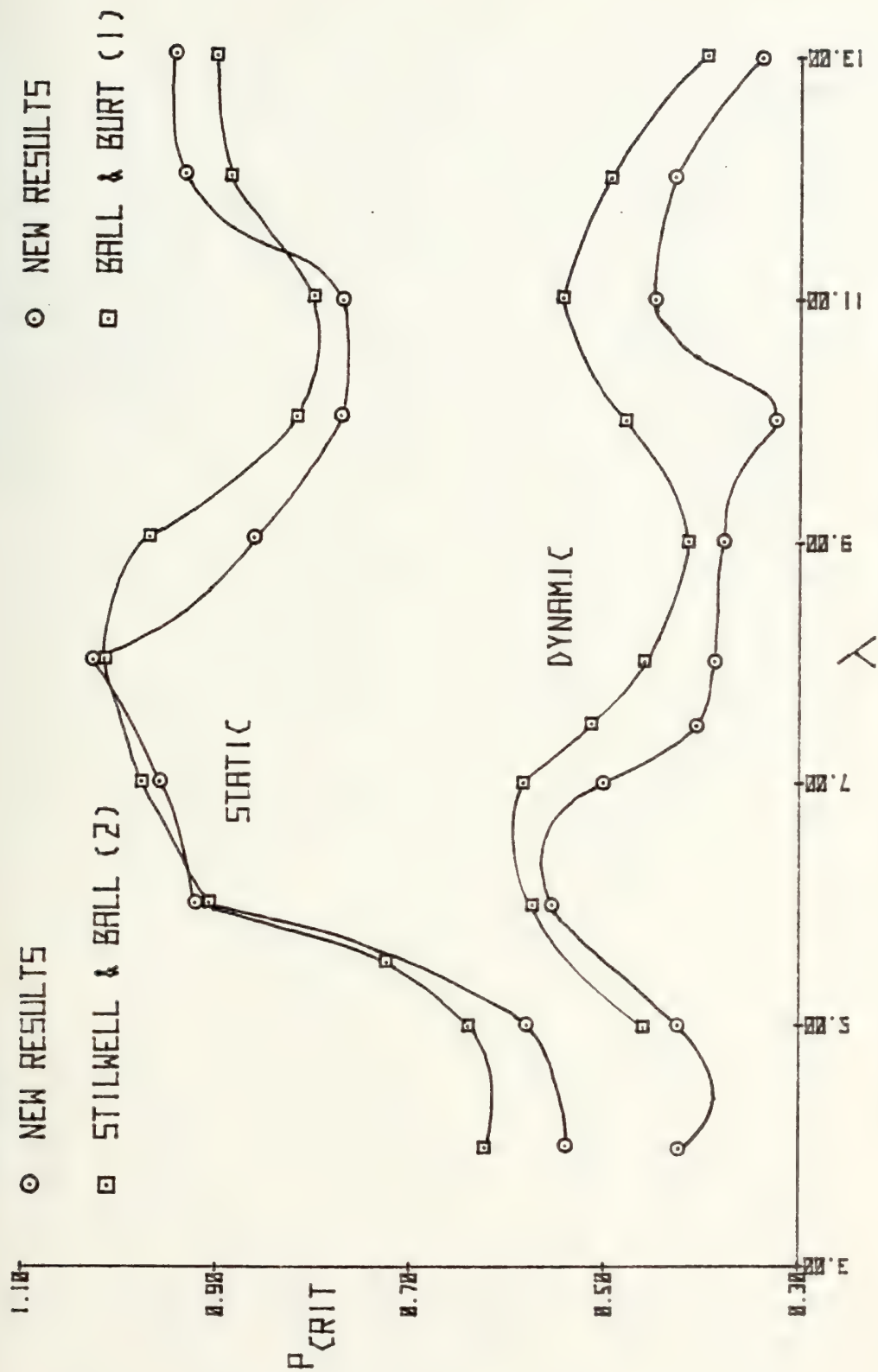


Figure 1 - CRITICAL STEP-PRESSURE LOAD VERSUS λ
 AXISYMMETRIC (SATANS-I VERSUS SATANS-IIA)

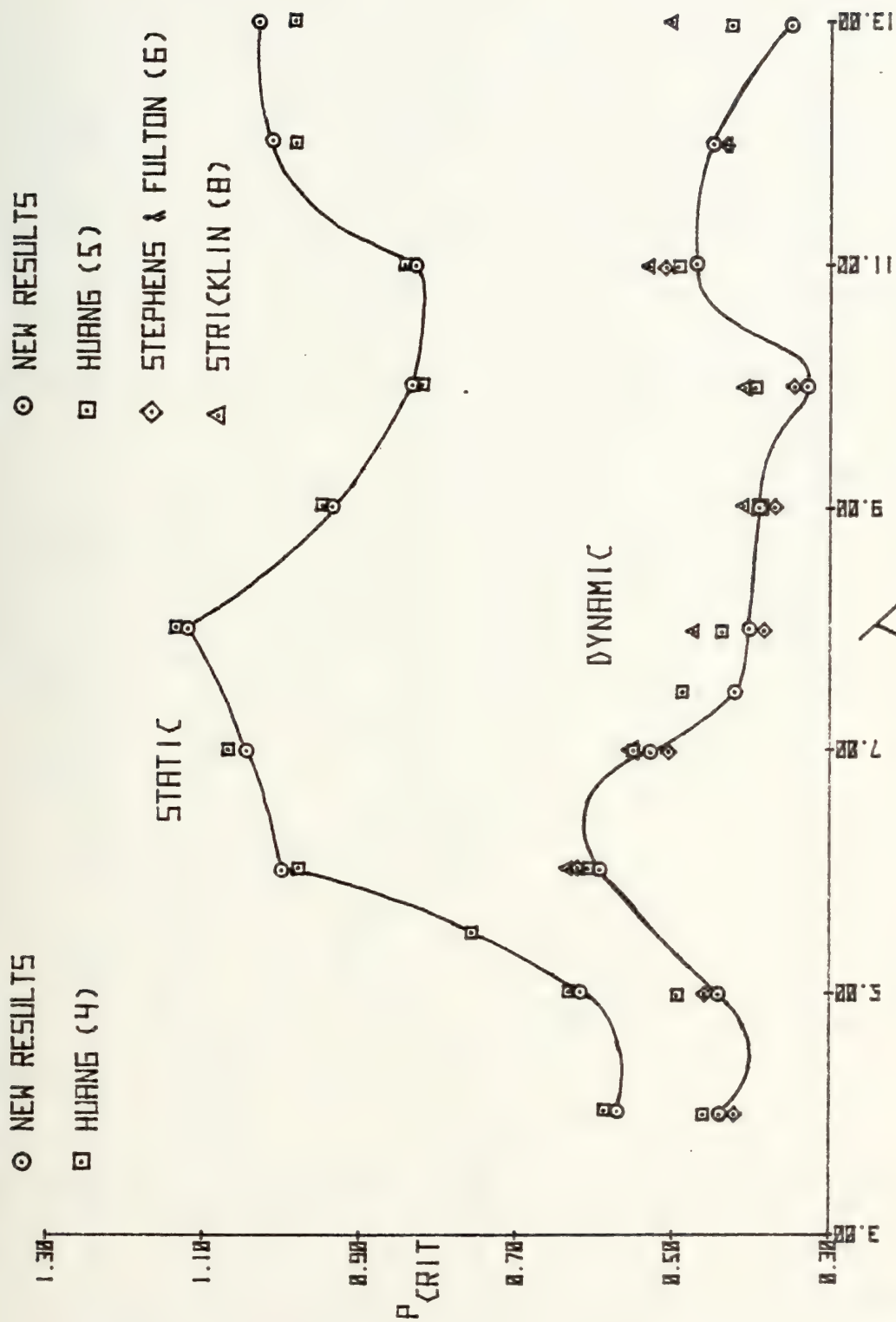


Figure 2 - CRITICAL STEP-PRESSURE LOAD VERSUS λ
 AXISYMMETRIC (SATANS-IIA VERSUS ALL OTHERS)

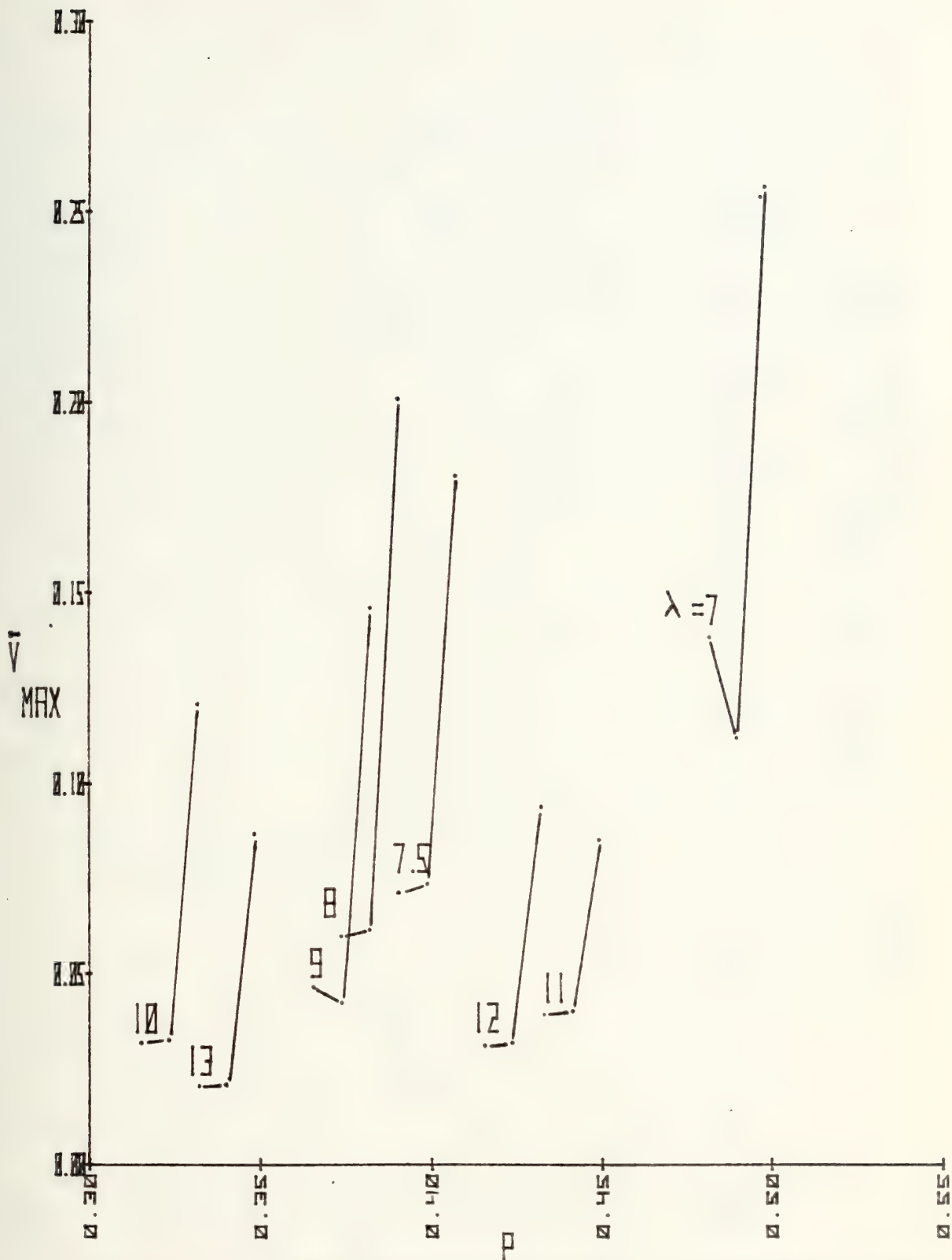


Figure 3 - PEAK DEFLECTION VERSUS P , AXISYMMETRIC AND ASYMMETRIC CASES FOR VARIOUS VALUES OF λ (SATANS-IIA)

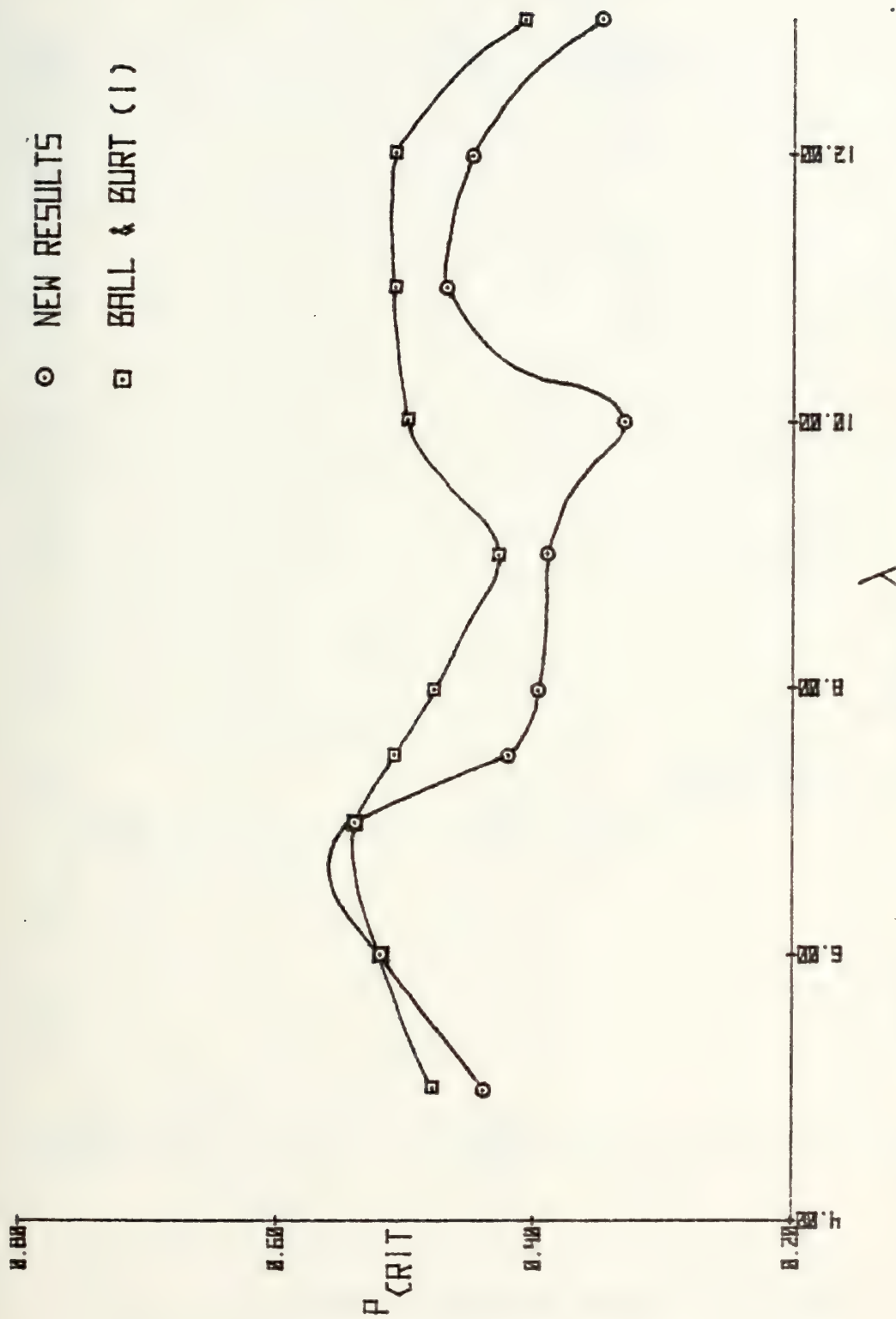
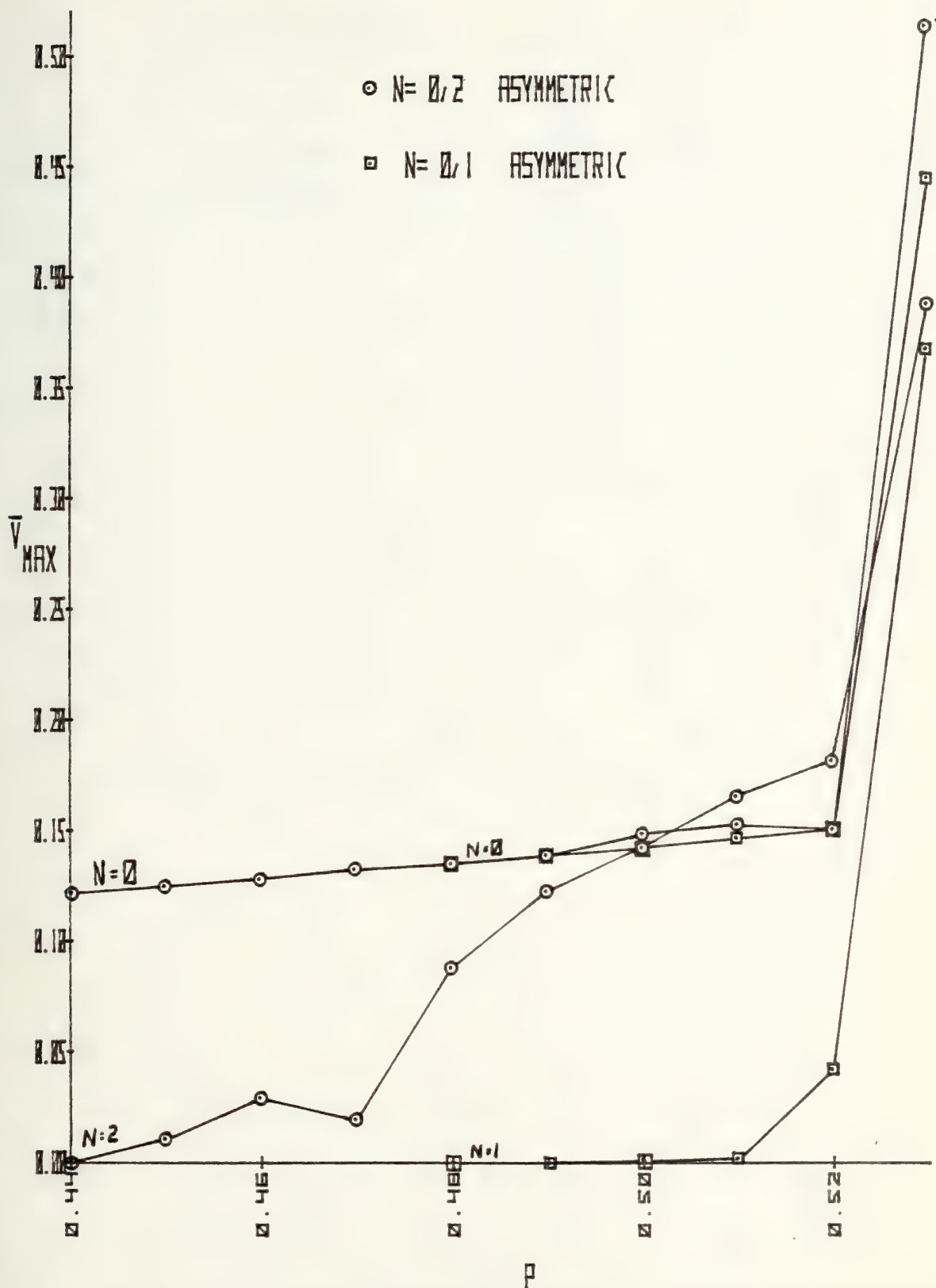


Figure 4 - CRITICAL STEP-PRESSURE LOAD VERSUS λ
ASYMMETRIC ANALYSES (SATANS-I VERSUS SATANS-IIA)



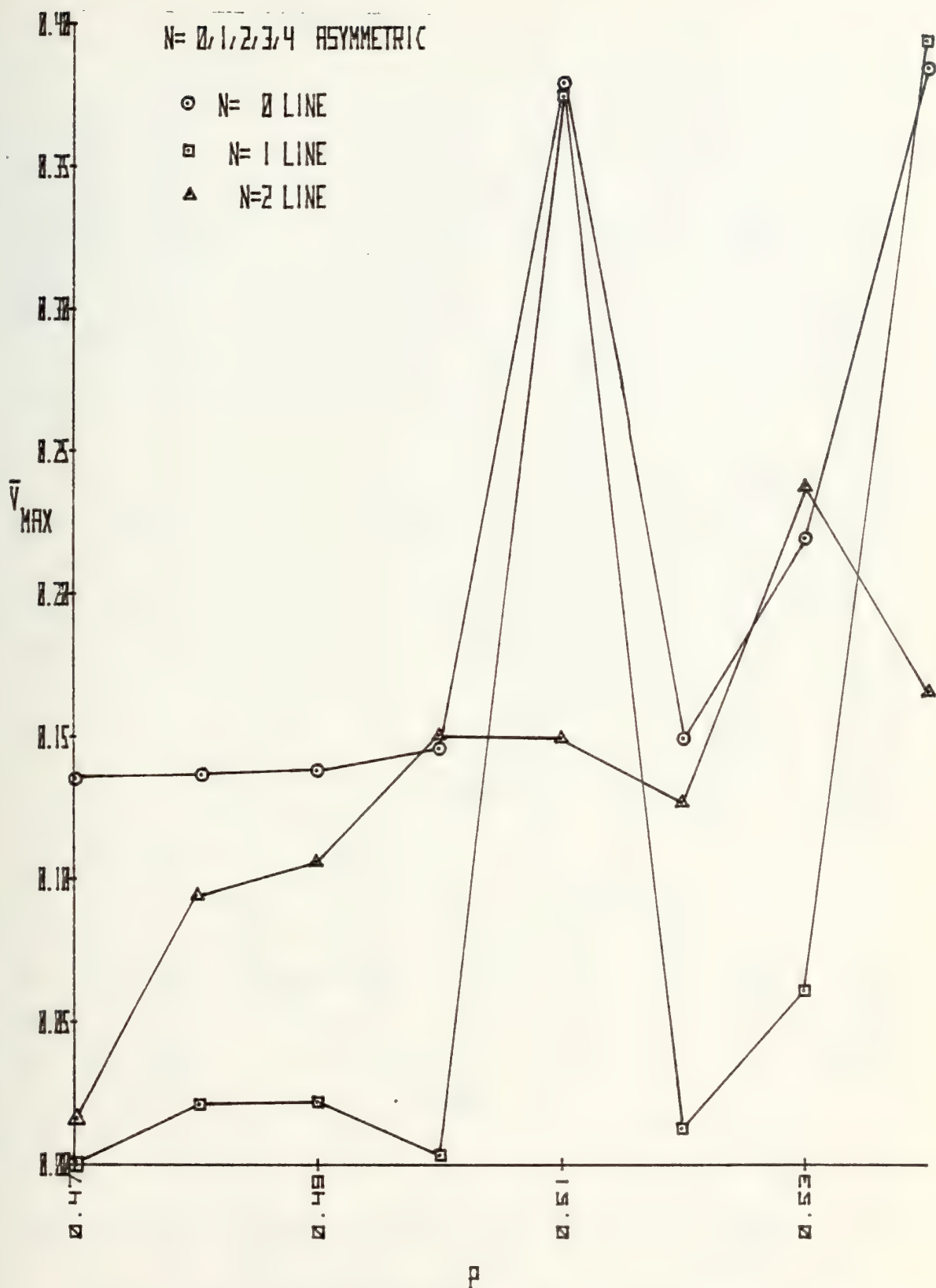


Figure 6 - PEAK DEFLECTION VERSUS P FOR THE ASYMMETRIC ANALYSES OF $\lambda = 6$ (N=0,1,2,3,AND4, ONLY N=0,1,AND2 PLOTTED)

NEW RESULTS

STRICKLIN (8)

LOCK, ET AL. (7)

AKKAS (9)

○ ASYMMETRIC

— AXISYMMETRIC

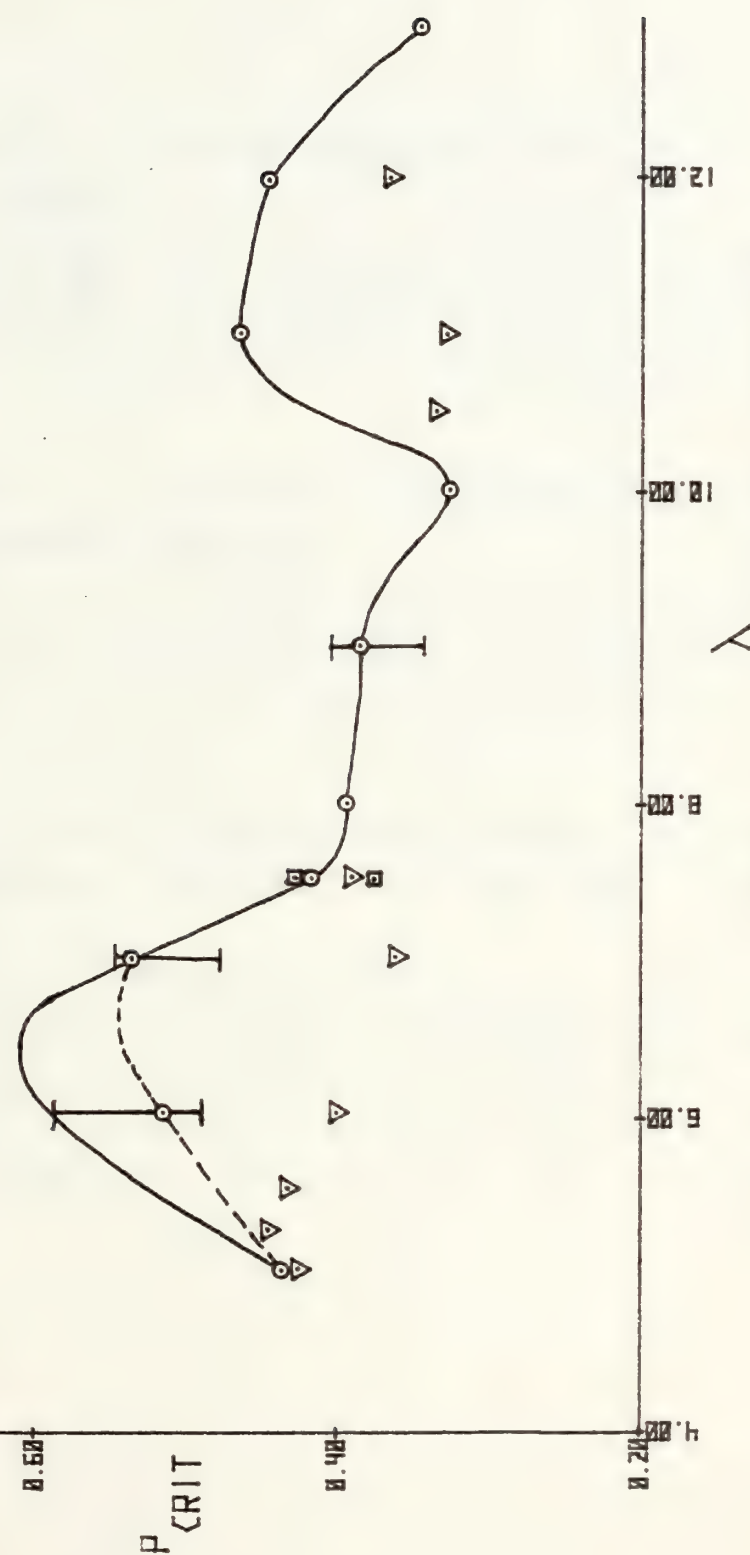


Figure 7 - CRITICAL STEP-PRESSURE LOAD VERSUS λ
ASYMMETRIC ANALYSES (SATANS-IIA VERSUS ALL OTHERS)

A. TABLES

1. TABLE I Critical pressure loads from the static axisymmetric analyses.

λ	4	5	6	7	8	9	10	11	12	13
P_{CRIT}	.568	.616	1.0	1.048	1.12	.936	.832	.832	1.016	1.032

2. TABLE II Critical step-pressure loads from the axisymmetric dynamic analyses.

λ	4	5	6	7	7.5	8	9	10	11	12	13
P_{CRIT}	.45	.44	.59	.53	.42	.40	.39	.33	.47	.45	.35

3. TABLE III Critical step-pressure loads from the dynamic asymmetric analyses and critical asymmetric harmonics.

λ	5	6	7	7.5	8	9	10	11	12	13
P_{CRIT}	.44	.52	.54	.42	.40	.39	.33	.47	.45	.35
N_{CRIT}	1	2	3	3	4	5	6	7	8	9

4. TABLE IV Dynamic asymmetric analyses for \bar{V}_{MAX} versus

P.

1. TABLE IV A. Two-harmonic analyses for all values of λ except $\lambda = 6$.

$\lambda = 5$ N= 0 and 2

N= 0 and 1

P	.43	.44	.45	P	.44	.45
N= 0	.1659	.1676	.6606	N= 0	.1675	.6606
N= 2	.0004787	.0000566	.0687	N= 1	.0003145	.0687
				P	.46	
				N= 0	.7653	
				N= 1	.001092	

$\lambda = 7$, N= 0 and 3

P	.45	.46	.47	.48	.49	.50	.52
N= 0	.09452	.09571	.09812	.1005	.1029	.1052	.1099
N= 3	.000889	.007456	.05052	.04323	.0279	.0335	.07488
P	.53	.54	.55				
N= 0	.1122	.1146	.2709				
N= 3	.05997	.06252	.03809				

$\lambda = 7.5$, N= 0 and 3

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2636	.07837	.2076
N= 3	.0001094	.001296	.0004304	.002754	.001188	.000338
P	.46					
N= 0	.200					
N= 3	.0003276					

$\lambda = 8, N= 0 \text{ and } 4$

P	.38	.39	.40	.41	.42	.43
N= 0	.05893	.0607	.0624	.1964	.1713	.1957
N= 4	.0000566	.0000703	.0000364	.0000333	.0000274	.0000299
P	.44					
N= 0	.2297					
N= 4	.0000326					

$\lambda = 9 N= 0 \text{ and } 4$

$N= 0 \text{ and } 5$

P	.38	.39	.40	P	.40
N= 0	.04738	.04875	.1576	N= 0	.05012
N= 4	.00003597	.00004635	.00004497	N= 5	.00008385

$\lambda = 10, N= 0 \text{ and } 5$

P	.32	.33	.34	.36	.38	.40
N= 0	.03239	.03347	.1086	.1217	.1288	.1235
N= 5	.0000281	.0000472	.00004125	.00002103	.0000449	.000114

$\lambda = 11, N= 0 \text{ and } 6$

P	.45	.46	.46	.48	.49	.50
N= 0	.03910	.04004	.04099	.09814	.04241	.08824
N= 6	.004595	.01332	.02232	.02864	.03955	.02813

$\lambda = 12, N= 0 \text{ and } 7$

P	.44	.45	.46
N= 0	.03236	.03316	.08633
N= 7	.00004214	.0004561	.00005158

$\lambda = 13, N= 0 \text{ and } 8$

P	.34	.35	.36	.38	.40
N= 0	.02119	.02185	.06637	.07844	.07381
N= 8	.00001148	.00001134	.000006607	.000008245	.000119

2. TABLE IV B. Two-harmonic analyses with $N=0$ and 1 ,
 $\lambda = 6$ only.

P	.48	.49	.50	.51	.52	.53
N= 0	.1350	.1385	.1421	.1460	.1499	.4453
N= 1	.0002797	.000195	.000245	.000926	.04081	.3668

3. TABLE IV C. Two-harmonic analyses with $N=0$ and 2 ,
 $\lambda = 6$ only.

P	.44	.45	.46	.47	.48	.49	.50
N= 0	.1218	.1250	.1276	.1320	.1350	.1385	.1479
N= 2	.000239	.0101	.0293	.01976	.08768	.1223	.1419
P	.51	.52	.53	.54	.55	.56	
N= 0	.1526	.1499	.5137	.5060	.2040	.5305	
N= 2	.1654	.1816	.3878	.3996	.2156	.3617	

4. TABLE IV D Five-harmonic analyses for selected
shells.

$\lambda = 6$ $N=0,1,2,3$, and 4

P	.47	.48	.49	.50	.51	.52	.53
N= 0	.1313	.1347	.1382	.1460	.3797	.1498	.2200
N= 1	.00021	.02108	.02215	.003676	.3743	.01276	.0616
N= 2	.0187	.0953	.1069	.1507	.1502	.1279	.2385
N= 3	.000181	.006237	.01437	.00163	.0405	.0123	.03978
N= 4	.0031	.04757	.05428	.04402	.05896	.0495	.064
P	.54						
N= 0	.3854						
N= 1	.3953						
N= 2	.1671						
N= 3	.05298						
N= 4	.0613						

$\lambda = 7.5$ $N = 0, 1, 2, 3, 4$ and 4

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2592	.07837	.2544
N= 1	.00004855	.00004198	.00006093	.0002737	.0001167	.005952
N= 2	.0001164	.00007456	.0004184	.0000982	.000788	.0003188
N= 3	.0001277	.001187	.0004597	.0002853	.00107	.0003188
N= 4	.0008224	.0001898	.0002448	.0000526	.000280	.000134

$\lambda = 11$ $N = 0, 4, 5, 6,$ and 7

P	.45	.46	.47	.48	.49	.50
N= 0	.03910	.04004	.0499	.04195	.04291	.1040
N= 4	.0005759	.001263	.0009774	.001388	.002657	.001565
N= 5	.009568	.0140	.0124	.02239	.02759	.01548
N= 6	.002560	.007828	.02330	.02767	.02602	.02644
N= 7	.0001743	.0001486	.0002021	.01202	.02048	.02064

APPENDIX A

LISTING OF SATANS-IIA


```

C ***** THIS SUBROUTINE COMPUTES THE NONDIMENSIONAL IN-PLANE AND
C BENDING STIFFNESSES OF THE SHELL *****
C ***** REAL NU, LAM2, JAY, MT, LSD18, LSCIN *****
C ***** CCMMCN /BL15/ NU, U1(99), V1(99), W1(99), V2(99), U2(99), W2(99), U3(99),
1 CCMMCN /BL17/ V3(99), W3(99) *****
C ***** CCMMCN /BL32/ TKN, ELAST, CHAR, SIGC *****
C ***** B=1.C89C82 *****
C ***** C=.C5C15683 *****
C ***** DE=C. *****
C ***** CC=0. *****
C ***** RETURN *****
C ***** END *****

```

*SAT00400
*SAT00410
*SAT00420
*SAT00430
*SAT00440
*SAT00450
*SAT00460
*SAT00470

```

C ***** SLPROUTINE PLOAD(K,Z) *****
C ***** THIS SUBROUTINE ESTABLISHES THE NON-DIMENSIONAL FCURIER *****
C ***** COEFFICIENTS OF THE LOADS APPLIED TO THE SHELL *****
C ***** REAL MASS *****
C ***** DIMENSION Z(4,1) *****
C ***** CCMMCN /IBL1/ MNMAX *****
C ***** CCMMCN /IBL2/ NN(99), MNINIT *****
C ***** CCMMCN /IBL4/ KMAX, KLITR *****
C ***** CCMMCN /IBL8/ LSTEP, PR(99), PX(99), PT(99) *****
C ***** CCMMCN /BL3/ SOE, OSE, ALOAD *****
C ***** CCMMCN /BL6/ R(500), GAM(500), QMT(500) *****
C ***** CCMMCN /BL8/ TKN, ELAST, CHAR, SIGC *****
C ***** CCMMCN /BL32/ DELCAD *****
C ***** CCMMCN /BL102/ MASS(500) *****
C ***** CCMMCN /BL103/ DEL/BL100/TEEO, $DYNMC *****
C ***** CCMMCN /BL17/DEL/BL100/TEEO, $DYNMC *****
C ***** CCMMCN /BLTHTA/ THTAM, COEFF *****
C ***** RETURN *****

```

SAT00520
SAT00530
SAT00540
SAT00550
SAT00560
SAT00570
SAT00580
SAT00590
SAT00600
SAT00610
SAT00620
SAT00630
SAT00640
SAT00650
SAT00660
SAT00670
SAT00680
SAT00690
SAT00700
SAT00710
SAT00720

```

C ***** SLPROUTINE INITL (Z,ZC,Z2,Z3,ZCCT) *****
C ***** THIS SUBROUTINE DESCRIBES THE INITIAL CONDTICNS FOR DYNAMIC CASES *****
C ***** IMPLICIT LOGICAL*1 ($) *****
C ***** DIMENSION Z(4,1), ZC(4,1), Z2(4,1), Z3(4,1), ZCCT(4,1) *****
C ***** CCMMCN /IBL1/ MNMAX *****
C ***** CCMMCN /IBL2/ NN(99), MNINIT *****
C ***** CCMMCN /IBL4/ KMAX, KL *****
C ***** CCMMCN /IBL5/ MAXM *****
C ***** CCMMCN /IBL12/ KMAX1, KMAX2, NCONV *****
C ***** CCMMCN /BL6/ SOE, CSE, ALOAD *****

```

SAT00910
SAT00920
SAT01110
SAT01120
SAT01130
SAT01140
SAT01150
SAT01160
SAT01170
SAT01180
SAT01190
SAT01200
SAT01210
SAT01220


```

CCMMCN /BL32/ TKN,ELAST,CHAR,SIGC
CCMMCN /BL100/ TEEC,$DYNMC
CCMMCN /BL101/ DELSD
NN(1)=0
NN(2)=1
NN(3)=2
NN(4)=4
PI=3.14159
CC Z N=1,MAXM
IF(N.EQ.1) VEL=-444.08/PI
IF(N.EQ.2) VEL=-444.08/2
IF(N.EQ.3) VEL=-444.08*2./((3.*PI))
IF(N.EQ.4) VEL=-444.08*2./((15.*PI))
IF(N.EQ.4) VEL= 444.08*2./((15.*PI))
CC Z K=2,KL
I=K+1+(N-1)*KMAX2
2 ZCCT(3,I)=VEL*ELAST*TEEO/(CHAR*SIGC)*10
RETURN

```

```

C*****
C***** TLOAD(K,Z)
C***** THIS SUBROUTINE DESCRIBES THE THERMAL LOADING CN THE SHELL
C*****
C*****
REAL NU
DIMENSION Z(4,1),MNMNAX
CCMMCN /IBL1/ MNMAX
CCMMCN /IBL2/ NN(99),MNINIT
CCMMCN /BL15/ NU,U1(99),V1(99),W1(99),U2(99),V2(99),W2(99),U3(99),
1 V3(99),W3(99)
CCMMCN /BL32/ TKN,ELAST,CHAR,SIGC
CCMMCN /IBL8/ LSTEP,ITR
CCMMCN /BL5/ TT(99),EMT(99),DT(59),DMT(99)
CCMMCN /BL6/ SOE,OSE,ALOAD
RETURN
ENC
SUBROUTINE IMPERF (PHIXB,PHITB)
DIMENSION PHIXB(1),PHITB(1)
CCMMCN /IBL4/ KMAX,KL
CCMMCN /IBL9/ MAXM
KANCM=KMAX*MAXM
CC I=1,KANDM
PHIXB(I)=0.
PHITB(I)=0.
CCATTINUE
1 RETURN
ENC
SUBROUTINE SATANS (P,CEE,DST,X,Z,ZC,Z2,Z3,ZCCT,IS,JS,ID,JD,PHIXB,

```

SAT01230
SAT01240
SAT01250

SAT01260
SAT01270
SAT00940
SAT00950
SAT00960
SAT00970
SAT00980
SAT00990
SAT01000
SAT01010
SAT01020
SAT01030
SAT01040
SAT01050
SAT01060
SAT01070
SAT01080
SAT01090
SAT01100
SAT01280
SAT01290

SAT01300
SAT01310
SAT01320


```

IP+ITB)
C** THIS SUBROUTINE READS ALL DATA, PRINTS THE OUTPUT TITLE PAGE,
C** AND PASSES CONTROL TO ONE OF THE MAJOR CCNTFCLLNG SLEROUTINES
C**
C** INFLICIT LCGICAL*1 ($)
REAL*4 NU,LAM,LAM2,JAY,MT,LSD18,LSCLN,MASS
DIMENSION P(4,4,1),DEE(4,4,1),X(4,1),Z(4,1),IC(99,1),
ZJC(99,1),PHIXB(1),PHITB(1)
CCMNCN /IBL1/ MNMAX
CCMNCN /IBL4/ KMAX,KL
CCMNCN /IBL5/ IBCINL,IBCFNL
CCMNCN /IBL9/ MAXM
CCMNCN /IBL10/ IFREQ,NTHMAX
CCMNCN /IBL13/ ITRMAX,LSMAX
1/IBLJ/ JUMP
CCMNCN /BL13/ OMEG1(4,4),CAPL1(4,4),OMEG1(4,4),CAPLL(4,4),
1 CCMNCN /BL15/ UNIT(4,4)
1 CCMNCN /BL15/ NU,U1(99),V1(99),W1(99),V2(99),U2(99),W2(99),U3(99),
CCMNCN /BL16/ EPS
CCMNCN /BL18/ ELL(4),ELL(4)
CCMNCN /BL19/ TH(36)
CCMNCN /BL32/ TKN,ELAST,CHAR,SIGC
CCMNCN /BL100/ TEEC,$DYNMC
CCMNCN /BL102/ DELCAD
CCMNCN /BLPLOT/ IRADII,IGAMMA,ICMEGS,IOMEGT,ICEOMS,IBSTIF,IDSTIF,
1 IBBSTF,IDDSTF,IPR,IPS,IP1,IT,IMT,IOIT,INS,
2 INTH,INSTH,IQS,IMS,IMTH,IMSTH,IU,IV,IW,IPHIS,
3 IPHIT,IPHI,$PLOTS,$MCDAL
CCMNCN /BLDATA/ TITLE,NO,IMODE,NDIMEN,IPRINT,LCHMAX,IC
CCMNCN /BLRUN/ IRNAGN
DIMENSION TITLE(18)
C** REAC IN DATA FOR THIS RUN
C**
C** REAC (5,100) TITLE
C** REAC (5,101) NO,$CYNMC,IMODE,NDIMEN,NTHMAX,IFREQ,IFRINT,IBCFNL,
1 IBCFNL,KMAX,MNMAX,MAXM,LSMAX,LCHMAX,ITRMAX,IC
C** REAC (5,102) NU,SIGC,ELAST,TKN,CHAR,TEEO
C** REAC (5,103) DELOAD,EPS
C** IF (NTHMAX.EQ.0) GC TO 1
C** REAC (5,104) (TH(NTH),NTH=1,NTHMAX)
C** CC 2 NTH=1,NTHMAX
C** TF(NTH)=TF(NTH)*6.2831853/360.0
1 IF (IBCFNL.EQ.0) READ (5,105) OMEG1,CAPL1,ELL

```



```

1C5 FCFMAT (4E16.8)
1C6 FCFMAT (2L2,29I2)
1C7 FCFMAT (I2)
C** ***** FCFMATS FOLLOW *****
C** WRITE STATEMENT FCFMATS FOLLOW *****
C** ***** FCFMATS FOLLOW *****
2C0 FCFMAT (I1,48X,---PRCBLE NUMBER,I5,---,///)
2C1 FCFMAT (I1,38X,18A4,///)
2C2 FCFMAT (I1,49X,---INPUT DATA RECCD---,///)
2C3 FCFMAT (I1,110,THE SHELL HAS AN INITIAL PCLE,/)
2C4 FCFMAT (I1,110,AT THE INITIAL EDGE,///2X,---CMEGA BARSAT02880
1AR-----,15X,---LAMD BAR-----,1SAT02890
22X,---EL-----,/)
2C5 FCFMAT (I1,4E10.3,') NS (I1,4E10.3,') U 'E10SAT02910
1.3)
2C6 FCFMAT (I1,4E10.3,') NST + (I1,4E10.3,') V = 'E10SAT02930
1.3)
2C7 FCFMAT (I1,4E10.3,') CS (I1,4E10.3,') W 'E10SAT02940
1.3)
2C8 FCFMAT (I1,4E10.3,') PHIS (I1,4E10.3,') MS 'E10SAT02960
1.3)
209 FCFMAT (I1,110,THE SHELL HAS A FINAL PCLE,/)
210 FCFMAT (I1,110,AT THE FINAL EDGE,///2X,---OMEGA BARSAT03000
1-----,15X,---LAMD BAR-----,12SAT03010
2X,---EL-----,/)
211 FCFMAT (///)
212 FCFMAT (I1,4X,NUMBER OF STATIONS-----,13/5X,INCREMENTAL LOAD FSAT03040
NUMBER OF MODES-----,F6.3/5X,MAXIMUM NUMBER OF ITERATIONCS-----,13/5X,MSAT03070
2ACTCR-----,I3/5X,MAXIMUM NUMBER OF FACTOR CHANGES-----,I3/5X,CCNVERGENCE CRITERSAT03090
3-----,F6.4//)
4AXIMUM NUMBER OF LOAD FACTOR CHANGES-----,F6.4//)
5ICN-----
213 FCFMAT (I1,4X,CHARACTERISTIC SHELL DIMENSION-----,E12.4/5X,REFERENCE ELSAT03100
1,REFERENCE THICKNESS-----,E12.4/5X,REFERENCE STRESS-----,E12.4/5X,REFERENCE ELSAT03110
2ASTICITY-----,E12.4/5X,PCISSONS RATIO-----,E12.4/5X,REFERENCE STRESS-----,E12.4/5X,REFERENCE ELSAT03120
3-----,E12.4/5X,PCISSONS RATIO-----,E12.4/5X,REFERENCE STRESS-----,E12.4/5X,REFERENCE ELSAT03130
4, E12.4//)
214 FCFMAT (I1,110,PLCTS HAVE BEEN REQUESTED FOR THE BELCW LISTED GESAT03140
1CNMETRY, STIFFNESS OR LOADING QUANTITIES:/)
215 FCFMAT (I1,170,RADIUS,/)
216 FCFMAT (I1,170,GAMMA,/)
217 FCFMAT (I1,170,GAMMA,/)
218 FCFMAT (I1,170,CMEGA-THETA,/)
219 FCFMAT (I1,170,CMEGA-THETA,/)
220 FCFMAT (I1,170,DECMEGA-S,/)
221 FCFMAT (I1,170,B-STIFFNESS,/)
222 FCFMAT (I1,170,B-PRIME,/)

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C      NESSES,LOADING (PHYSICAL AND/OR THERMAL), AND INITIAL CCNTIDICNS.*SAT03730
C      IT CCNTIDICNS PROBLEM SOLUTION PROCEDURE.*SAT03740
C      *****SAT03750
C      INPLICIT LCGICAL*1 ($)*****SAT03760
C      REAL*4 NU,LAM2,JAY,MT,LSD18,LSCIN,MASS*****SAT03770
C      DIMENSION P(4,4,1),DEE(4,4,1),DST(4,4,1),X(4,1),Z(4,1),*****SAT03780
C      1ZC(4,1),Z2(4,1),Z3(4,1),ZDOT(4,1),IS(99,1),JS(99,1),IC(55,1),*****SAT03790
C      2JC(55,1),PHIXB(1),PHITB(1)*****SAT03800
C      CCMMCN /IBL1/ MNMAX*****SAT03810
C      CCMMCN /IBL2/ N(99),MNINIT*****SAT03820
C      CCMMCN /IBL3/ .N, APPEARS AS .NN. IN SUBROUTINES PLCAD & EFG*****SAT03830
C      CCMMCN /IBL4/ MO,M1,M2,M3*****SAT03840
C      CCMMCN /IBL5/ KMAX,KL*****SAT03850
C      CCMMCN /IBL6/ IBCINL,IBCFNL*****SAT03860
C      CCMMCN /IBL7/ KLL*****SAT03870
C      CCMMCN /IBL8/ MNMAXC,MAXD(99),MAXS(99),MAXSY(99),IJS(99)*****SAT03880
C      CCMMCN /IBL9/ LSTEP,ITR*****SAT03890
C      CCMMCN /IBL10/ MAXM*****SAT03900
C      CCMMCN /IBL11/ IFRREG,NTHMAX*****SAT03910
C      CCMMCN /IBL12/ ICORFL,IPASS*****SAT03920
C      CCMMCN /IBL13/ KMAX1,KMAX2,ACCNV*****SAT03930
C      CCMMCN /BL1/ ITRMAX,LSMAX,A(4,4),BEE(4,4),C(4,4)*****SAT03940
C      CCMMCN /BL3/ PR(99),PX(99),PT(99),ZF2M(4,4,99),*****SAT03950
C      CCMMCN /BL4/ ZF1M(4,4,99),ZF4M(4,4,99),*****SAT03960
C      1 CCMMCN /BL5/ ZF3M(4,4,99),ZF4M(4,4,99),*****SAT03990
C      CCMMCN /BL6/ DT(99),MT(99),AS,EMT, IN SUBROUTINES INLPOL & FNLPOL*****SAT04000
C      CCMMCN /BL7/ .MT, APPEARS AS .EMT, IN SUBROUTINES INLPOL & FNLPOL*****SAT04010
C      CCMMCN /BL8/ SOE,CSE,ALOAD*****SAT04020
C      CCMMCN /BL9/ DI,SI*****SAT04030
C      CCMMCN /BL10/ R(500),GAM(500),DMT(500)*****SAT04050
C      CCMMCN /BL11/ FFS(4,99),ELIS(4),GEES(4,99)*****SAT04060
C      CCMMCN /BL12/ PHIX(99),PHIT(99),PHI(99)*****SAT04070
C      CCMMCN /BL13/ QMXI(500),PHEE,T0,T2*****SAT04080
C      1 CCMMCN /BL14/ TDLI,TDEL*****SAT04090
C      CCMMCN /BL15/ OMEGI(4,4),CAPL1(4,4),OMEGL(4,4),CAPLL(4,4),*****SAT04100
C      CCMMCN /BL16/ UNIT(4,4)*****SAT04110
C      CCMMCN /BL17/ LAM2,LSD18,LSDIN*****SAT04120
C      CCMMCN /BL18/ NU,UI(99),V1(99),W1(99),V2(99),U2(99),U3(99),*****SAT04130
C      CCMMCN /BL19/ V3(99),W3(99)*****SAT04140
C      CCMMCN /BL20/ EPS*****SAT04150
C      CCMMCN /BL21/ DEL*****SAT04160
C      CCMMCN /BL22/ ELI(4),ELL(4)*****SAT04170
C      CCMMCN /BL23/ TH(36)*****SAT04180
C      CCMMCN /BL24/ DEQMX(500)*****SAT04190
C      CCMMCN /BL25/ JAY(4,4),H(4,4),*****SAT04200
C      CCMMCN /BL26/ DL(4,4,99),DG(4,4,99),DF(4,4,99)*****SAT04210
C      CCMMCN /BL27/ E(4,4),F(4,4),G(4,4)*****SAT04220

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CCMCN /BL27/ BX3(99),BT3(99),BXT2(99),BE3(99) SAT04210
CCMCN /BL28/ EXX3(99),ETT3(99),ETX3(99),EX3(99),ET3(99) SAT04220
CCMCN /BL29/ BX1(99),BT1(99),BXT1(99),BE1(99),B12(99), SAT04230
1 BXT2(99),BE2(99) SAT04240
1 CCMCN /BL30/ EXX1(99),ETT1(99),ETX1(99),EX1(99),ET1(99),EXX2(99), SAT04250
ETT2(99),ETX2(99),EXT2(99),EX2(99),ET2(99) SAT04260
CCMCN /BL31/ DELSQ,EXT1(99) SAT04270
CCMCN /BL32/ TKN,ELAST,CHAR,SIGC SAT04280
CCMCN /BL100/ TEEQ,$DYNMC SAT04290
CCMCN /BL101/ DELSCD SAT04300
CCMCN /BL102/ DELCAD SAT04310
CCMCN /BL103/ MASS(500) SAT04320
CCMCN /BL110/ TX(99),TTH(99),TXT(99),MX(99),MTH(99),MXT(99), SAT04330
1 QS(99) SAT04340
CCMCN /BL111/ ABZ,ABZ0,ABZN,ABZ3,CD2 SAT04350
CCMCN /BLPHS/ PHX(99)
CCMCN /BLPLOT/ IRAD11,IGAMMA,ICMEGS,IOMEGT,IDECMS,IBSTIF,IDSTIF, SAT04360
1 IBBSTF,IBDSTF,IPR,IPS,IPI,IIT,IMT,ICIT,ICMT,INS, SAT04370
2 INTH,INTH,IQS,INS,IMH,IMSTF,IU,IV,IW,IHIS, SAT04380
3 IPHIT,IPH1,$PLOTS,$MODAL SAT04390
CCMCN /BLPLT1/ XRAC11(200),YGMMA(200),YCMEGS(200),YCMEGT(200), SAT04400
1 YDECMS(200),YBSTIF(200),YDSTIF(200),YBBSIF(200), SAT04410
2 YDSTIF(200),YPR(200),YPS(200),YPT(200),YIT(200), SAT04420
3 YMT(200),YDIT(200),YDMT(200),YNS(200),YNTF(200), SAT04430
4 YNSTH(200),YQS(200),YMS(200),YMTH(200),YVSTH(200), SAT04440
5 YU(200),YV(200),YW(200),YPLIS(200),YPLIT(200), SAT04450
6 YPHI(200),XSTATN(200) SAT04460
CCMCN /BLDATA/ TTITLE,NO,IMODE,NCIMEN,IPRINT,LCHMAX,IC SAT04470
CIMPENSICN SIGT(2),SIGC(2),TTITLE(18) SAT04480
C***** SAT04490
WRITE (6,8888) SAT04500
CELSD=DELCAD*DELOAD SAT04510
KL=KMAX-1 SAT04520
KLL=KMAX-2 SAT04530
KMAX1=KMAX+1 SAT04540
KMAX2=KMAX+2 SAT04550
AK=KL SAT04560
SIGT(1)=SIGO*TKN SAT04570
SIGT(2)=SIGO/ELAST SAT04580
SIGC(1)=SIGO*CHAR/ELAST SAT04590
SIGC(2)=SIGO*TKN*3/CHAR SAT04600
IF (IBCNL.LT.0) GO TO 14 SAT04610
DO 58 I=1,4 SAT04620
CC 58 J=1,4 SAT04630
KKLM=J/4+1 SAT04640
CMEGI(1,J)=OMEGI(1,J)*SIGT(KKLM) SAT04650
CAPLI(1,J)=CAPLI(1,J)*SIGC(KKLM) SAT04660
98 IF (IBCFNL.LT.0) GO TO 17 SAT04670
14

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SAT04680
SAT04690
SAT04700
SAT04710
SAT04720
SAT04730
SAT04740
SAT04750
SAT04760
SAT04770
SAT04780
SAT04790
SAT04800
SAT04810
SAT04820
SAT04830
SAT04840

SAT04850
SAT04860
SAT04870
SAT04880
SAT04890
SAT04900
SAT04910
SAT04920
SAT04930
SAT04940
SAT04950
SAT04960
SAT04970
SAT04980
SAT04990
SAT05000
SAT05010
SAT05020
SAT05030
SAT05040
SAT05050
SAT05060
SAT05070
SAT05080
SAT05090
SAT05100
SAT05110
SAT05120
SAT05130

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CC 99 I=1,4
CC 99 J=1,4
KK LM=J/4+1
CMEGL(I,J)=OMEGL(I,J)*SIGT(KKLM)
CAPLL(I,J)=CAPLL(I,J)*SIGC(KKLM)
LAM=TKN/CHAR
LCE=SIGC/ELAST
CCE=.5*SOE
CI=1.0-NU
SI=1.0+NU
LAM2=LAM**2
IF(KDIMEN.LT.1) GC TO 228
SIGCC=1.0
ELAST=1.0
TKN=1.0
CFAR=1.0
CC 230 N=1,MAXM
PFX(M)=C.0
PFT(M)=C.0
PIN(M)=0.0
PX(M)=0.0
PT(M)=0.0
PR(M)=0.0
TI(M)=0.0
NT(M)=0.0
LT(M)=0.0
CNT(M)=C.0
MAXD(M)=0
MAXS(M)=0
MAXSY(M)=0
CALL GECM
ICFCK1=IABS(JGAMMA)+IABS(IOMEGS)+IABS(IOMEGT)+IABS(ICEOMS)
1 ICFCK2=IABS(IRADII)+IABS(IRADII)
ICFCK2=IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(ICDSTF)
IF (.NOT.$PLOTS) GC TO 1001
CC 2 K=1,KMAX
XSTATN(K)=FLOAT(K)
2 IF (ICFCK1.EQ.0) GO TO 1001
CC 1 K=1,KMAX
XRADII(K)=R(K)*CHAR
YGAMMA(K)=GAM(K)/CHAR
YCMEGS(K)=CMXI(K)/CHAR
YCMEGT(K)=CMT(K)/CHAR
YLECMS(K)=DEOMX(K)/(CHAR*CHAR)
1 CCNTINUE
1001 CC 86 K=1,KMAX
CC 86 MASS(K)=0.

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SAT051140
SAT051150
SAT051160
SAT051170
SAT051180
SAT051190
SAT05200
SAT05210
SAT05220
SAT05230
SAT05240
SAT05250
SAT05260
SAT05270
SAT05280
SAT05290
SAT05300
SAT05310
SAT05320
SAT05330
SAT05340
SAT05350
SAT05360
SAT05370
SAT05380
SAT05390
SAT05400
SAT05410
SAT05420
SAT05430
SAT05440
SAT05450
SAT05460
SAT05470
SAT05480
SAT05490
SAT05500
SAT05510
SAT05520
SAT05530
SAT05540
SAT05550
SAT05560
SAT05570
SAT05580
SAT05590
SAT05600
SAT05610

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WRITE(6,802)
CC 578 K=1,KMAX
RKK=R(K)*CHAR
CMXIK=CMXI(K)/CHAR
GAMK=GAM(K)/CHAR
CECMXK=CECMX(K)/((CHAR*CFAR)
WRITE(6,803) K,RKK,GAMK,CMXIK,OMTK,DECMXK
978
803
N1=0
N2=0
N3=0
AEN=CHAR/SIGQ/TKN
ZN=SIGQ*TKN
WRITE(6,112)
CC 888 K=1,KMAX
CALL BCE(K,B,DB,D,DD)
EST=ELAST*TKN
ZST=ELAST*TKN**3
B=B*BST
C=C*ZST
CB=CB/CHAR*BST
CC=CC/CHAR*ZST
WRITE(6,71) K,B,D,CB,DD
IF (.NOT.$PLCTS.OR.(ICCHK2.EQ.0)) GO TO 888
YES=IF(K)=B
YCSTIF(K)=C
YECSTIF(K)=CD
CCNTINLE
CALL PLCAD(1,Z)
CALL TLCAD(1,Z)
CC 889 N=1,MNMAX
WRITE(6,113) N(M)
WRITE(6,114)
ICCHK3=IABS(IPR)+IABS(IPS)+IABS(IPT)+IABS(ITT)+IABS(IMT)
1
DC 890 K=1,KMAX
CALL PLCAD(K,Z)
CALL TLCAD(K,Z)
PFM=PR(M)/ABN
PTM=PT(M)/ABN
FXM=PX(M)/ABN
TMM=TT(M)*ZN
ENTM=MT(M)/CHAR*ZN
DTM=DT(M)/CHAR*ZN
CMTM=DMT(M)*ZN*TKN/(CHAR*CHAR)
WRITE(6,115) K,PRM,PXM,PTM,ENTM,DTM,CMTM
888

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IF (.NCT.$PLCTS.GR.(ICHCK3.EQ.0)) GO TO 890
YPR(K)=PRM
YFS(K)=PXN
YPT(K)=PTM
YTT(K)=TTM
YMT(K)=ETM
YCTI(K)=DTM
YCMT(K)=DMTM
CCNTINUE
85C IF (M.EQ.1) ICHCK3=ICHCK1+ICHCK2+ICHCK3
IF ($PLCTS.AND.(ICHCK3.GT.0)) CALL PLOT1(M)
855 CCNTINUE
DELSQ=DEL#2
TCLI=.5/DEL
TCEL=2.C*DEL
MNNIT=1
MNNMAXC=MNNMAX
CC 20 I=1,4
CC 20 J=1,4
UNIT(I,J)=0.0
2C IF (I.EQ.J) UNIT(I,J)=1.0
NMAX=MXXM*KMAX2
CC 22 K=1,NMAX
CC 22 I=1,4
ZCCT(I,K)=0.0
ZC(I,K)=0.0
Z2(I,K)=0.0
Z3(I,K)=0.0
Z(I,K)=0.0
22 ALCAD=DELCAD
CALL IMPERF (PHIXB,PHITB)
CALL FMATRX (P,X,ZC,Z2,Z3,DEE,DST)
LSTEP=1
LCHANG=0
ITR=1
ICCRFL=0
IF (MNNMAX.EQ.MAXM) ICORFL=1
IPASS=0
CALL XANDZ (P,DEE,DST,X,Z,ZC,Z2,Z3,ZDOT,IS,JS,ID,JD,PTIXB,PHITB)
4CC IF (ITRMXX.EQ.1) GO TO 50
MNNMAXC=MNNMAX
IF (IPASS.LT.2) CALL MODES (IS,JS,IC,JD,P,X,ZC,Z2,Z3,DEE,DST)
IF ((INCONV.EQ.1).AND.(ITR.GT.1)) GO TO 50
IF (ITR.LT.ITRMAX) GC TO 23
IF (LCHANG.LT.LCHMAX) GO TO 30
WRITE(6,220) NO
GC TO 500
FL=LSTEP
5C

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SAT05620
 SAT05630
 SAT05640
 SAT05650
 SAT05660
 SAT05670
 SAT05680
 SAT05690
 SAT05700
 SAT05710
 SAT05720
 SAT05730
 SAT05740
 SAT05750
 SAT05760
 SAT05770
 SAT05780
 SAT05790
 SAT05800
 SAT05810
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 SAT05880
 SAT05890
 SAT05900
 SAT05910
 SAT05920
 SAT05930
 SAT05940
 SAT05950
 SAT05960
 SAT05970
 SAT05980
 SAT05990
 SAT06000
 SAT06010
 SAT06020

 SAT06040
 SAT06050
 SAT06060
 SAT06070
 SAT06080
 SAT06090


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FI=IPRINT
LI=LSTEP/IPRINT
FLI=LI
FT=FLI-FL/FI
1 ILC(JD,PI,XB,PHITB) CALL CPUTUT(IMCDE,P,CEE,DST,X,2,ZC,Z2,Z3,ZCCT,IS,JS,
IF(LSTEP.EQ.1) ITRPR=1
IF(LSTEP.EQ.1) ITRPR=1
IF(ITR.GT.ITRPR) ITRPR=ITR
IF(LSTEP.GE.LSMAX) GO TO 360
6C CC 61 MN=1,MNMAX
CC 61 K=1,KMAX2
IK=K+(MN-1)*KMAX2
CC 61 I=1,4
ZN=2.0+Z(I,IK)-ZC(I,IK)
ZC(I,IK)=Z(I,IK)
Z(I,IK)=ZN
61 IF(LSTEP.GE.LSMAX) GO TO 360
62 ALCAD=ALOAD+DELOAD
LSTEP=LSTEP+1
ITR=1
GC TO 4C0
36C WRITE(6,221) NO
GC TO 5C0
23 ITR=ITR+1
GC TO 4C0
3C IF(LSTEP-1) 310,310,320
310 WRITE(6,223)
GC TO 5C0
32C WRITE(6,222)
LCFANG=LCHANG+1
LSTEP=LSTEP-1
ALCAD=ALOAD-DELOAD
CC 32 MN=1,MNMAX
CC 32 K=1,KMAX2
IK=K+(MN-1)*KMAX2
CC 32 I=1,4
Z(I,IK)=ZC(I,IK)
32 GC TO 62
C*****
71 FCRMAT(20X,13,4X,4E20.6)
112 FCRMAT(///17X,12F B STIFFNESS 20H 20H 20H D ST SAT06510
1 IFFNESS 20H B PRIME //) SAT06520
113 FCRMAT(///25X,44HPRESSURE AND TEMPERATURE CCEFFICIENTS FOR N=13,8H SAT06530
1 FLOW//) SAT06540
114 FCRMAT(5X,7HSTATION,3X,15H PR 15H PX 15H DTT 15H SAT06550
1 PT 15H SAT06560
1 SAT06570

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25F DMT //)
115 FCFRMT(6X,I3,7X,7E15.4) THE MAXIMUM NUMBER CF LOAC CHANGES HAVE BEEN
22C FCFRMT(IH1,80H) THE MAXIMUM NUMBER CF LOAC STEPS HAVE BEEN
221 FCFRMT(IH1,79H) THE MAXIMUM NUMBER CF LOAC STEPS HAVE BEEN
222 FCFRMT(IH1,119H) THE SOLUTION DID NOT CONVERGE WITHIN THE MAXIMUM
15X NUMBER OF ITERATIONS. THE LOAD FACTOR HAS BEEN DIVIDED BY
25F FCFRMT(IH1,69H) THE SOLUTION DID NOT CONVERGE FOR THE FIRST
11X INCREMENT. //11X,71HLOOK FOR AN ERROR IN THE INPUT DATA, OR TRY A SMALLER VALUE FOR DELCAD.)
8C2 FCFRMT(IH1,17X,15H STATION 16H RACILS 16H GAMMA
16F OMEGA S 16H DECMEGA S //)
8C3 FCFRMT(20X,I3,9X,5E16.4)
888 FCFRMT(00,T20,EXECUTING IN SUBROUTINE "STATIC")
5CC RETURN
END
SUBROUTINE DYNAMC (P,CEE,DST,X,Z,ZC,Z2,Z3,ZCCT,IS,JS,ID,JD,PHIXB,
1PHITB)
C*****
C THIS SUBROUTINE IS ONE OF THE MAJOR CONTROLLING SUBROUTINES FOR
C ALL DYNAMIC ANALYSIS PROBLEMS. IT OPERATES IN A FASHION SIMILAR
C TO SUBROUTINE STATIC.
C*****
C IMPLICIT LOGICAL*1 ($)
REAL*4 NU,LAM,LAM2,JAY,MT,LSD18,LSDCN,MASS
DIMENSION P(4,4,1),CEE(4,4,1),DST(4,4,1),X(4,1),Z(4,1),
1ZC(4,1),Z2(4,1),Z3(4,1),ZDOT(4,1),JS(99,1),ID(99,1),
2JCC(99,1),PHIXB(1),PHITB(1)
C*****
C COMMON /IBL1/ MNMAX
C*****
C COMMON /IBL2/ N(99),MNIAT
C*****
C COMMON /IBL3/ MO,M1,M2,M3
C*****
C COMMON /IBL4/ KMAX,KL
C*****
C COMMON /IBL5/ IBCINL,IBCFNL
C*****
C COMMON /IBL6/ KLL
C*****
C COMMON /IBL7/ MNMAXO,MAXD(99),MAXS(99),MAXSY(99),IJS(99)
C*****
C COMMON /IBL8/ LSTEP,ITR
C*****
C COMMON /IBL9/ MAXM
C*****
C COMMON /IBL10/ IFREQ,NTHMAX
C*****
C COMMON /IBL11/ ICCRFL,IPASS
C*****
C COMMON /IBL12/ KMAX1,KMAX2,ACONV
C*****
C COMMON /IBL13/ ITRMAX,LSMAX
C*****
C COMMON /BL1/ A(4,4),BEE(4,4),C(4,4)
C*****
C COMMON /BL3/ PR(99),PX(99),ZF2M(4,4,99),
1 ZF1M(4,4,99),ZF4M(4,4,99),
ZF3M(4,4,99),ZF4M(4,4,99)
C*****

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CCMMCN	/BL5/	TT(99),MT(99),DT(99),DMT(99) MT APPEARS AS 'EMT' IN SUBROUTINES INLPCL & FNLPOL	SAT07060
CCMMCN	/BL6/	SOE, QSE, ALOAD	SAT07070
CCMMCN	/BL7/	DL, SL	SAT07080
CCMMCN	/BL8/	R(500), GAM(500), QMT(500)	SAT07090
CCMMCN	/BL9/	FFS(4,99), ELIS(4), CEES(4,99)	SAT07100
CCMMCN	/BL10/	PHIX(99), PHIT(99), PFI(99)	
CCMMCN	/BL11/	OMXI(500), PHEE, IO, I2	SAT07120
CCMMCN	/BL12/	TOLII, TDEL	SAT07130
CCMMCN	/BL13/	OMEGI(4,4), CAPLI(4,4), OMEGL(4,4), CAPLL(4,4),	SAT07140
1		UNIT(4,4)	SAT07150
CCMMCN	/BL14/	LAM2, LSDL8, LSCIN	SAT07160
CCMMCN	/BL15/	NU, UI(99), VI(99), w1(99), V2(99), L2(99), w2(99), U3(99),	SAT07170
1		V3(99), w3(99)	SAT07180
CCMMCN	/BL16/	EPS	SAT07190
CCMMCN	/BL17/	DEL	SAT07200
CCMMCN	/BL18/	ELI(4), ELL(4)	SAT07210
CCMMCN	/BL19/	TH(36)	SAT07220
CCMMCN	/BL20/	DEOMX(500)	SAT07230
CCMMCN	/BL23/	JAY(4,4), F(4,4)	SAT07240
CCMMCN	/BL24/	DL(4,4,99), DG(4,4,99), DF(4,4,99)	SAT07250
CCMMCN	/BL25/	E(4,4), F(4,4), G(4,4)	
CCMMCN	/BL27/	BX3(99), BT3(99), BXT2(99), BE3(99)	SAT07270
CCMMCN	/BL28/	EXX3(99), ETI3(99), ETX3(99), EXI3(99), ET3(99)	SAT07280
CCMMCN	/BL29/	BX1(99), BT1(99), BXT1(99), BE1(99), BX2(99), BT2(99),	SAT07290
1		BXT2(99), BE2(99)	SAT07300
CCMMCN	/BL30/	EXX1(99), ETI1(99), ETX1(99), EXI1(99), ET1(99), EXX2(99),	SAT07310
1		ETT2(99), ETI2(99), ETX2(99), EXI2(99), ET2(99)	SAT07320
CCMMCN	/BL31/	DELSQ, EXI1(99)	SAT07330
CCMMCN	/BL32/	TKN, ELAST, CHAR, SIGC	SAT07340
CCMMCN	/BL100/	TEEG, \$DYNMC	SAT07350
CCMMCN	/BL101/	DELSQ	SAT07360
CCMMCN	/BL102/	DELOAD	SAT07370
CCMMCN	/BL103/	MASS(500)	SAT07380
CCMMCN	/BL110/	TX(99), TTH(99), TTX(99), MX(99), MTH(99), MXT(99),	SAT07390
1		QS(99)	SAT07400
CCMMCN	/BL111/	ABZ, ABZC, ABZN, ABZ3, DC2	SAT07410
CCMMCN	/BLPFS/	PHX(99), PHT(99)	SAT07420
CCMMCN	/BLFLCT/	IRACII, ICAMMA, ICMEGS, IOMEGT, ICEOMS, IBSTIF, IDSTIF,	SAT07430
		IBBSTF, IDBSTF, IPR, IPS, IPT, IIT, IMT, ICIT, ICM, INS,	SAT07440
1		INTH, INSTH, IQS, IMS, IMTH, INSTH, IU, IV, IW, IFHIS,	SAT07450
2		IPHIT, IPHI, \$PLOTS, \$MODAL	SAT07460
3		XRADII(200), YGAMMA(200), YCMEGS(200), YCMEGT(200),	SAT07470
CCMMCN	/BLPLTI/	YDECM(200), YBSTIF(200), YDSTIF(200), YBBSTF(200),	SAT07480
1		YDDSTF(200), YPR(200), YPS(200), YPT(200), YTT(20C),	SAT07490
2		YMT(200), YDT(20C), YDMT(200), YNS(200), YNTH(200),	SAT07500
3		YNSTH(200), YQS(200), YMS(200), YMTH(200), YMSTH(20C),	SAT07510
4		YL(200), YV(200), YW(200), YPHIS(200), YPFI(200),	SAT07520
5			


```

6  CCOMMON /BLDATA/ TITLE,NC,IMODE,NCIMEN,IPRINT,LCHMAX,IC
   DIMENSICN SIGT(2),SIGC(2),TITLE(18)
   *****
   C*****
   WRITE (6,8888)
   CELSD=DELCAD*DELCAC
   KLL=KMAX-1
   KLL=KMAX-2
   KMAX1=KMAX+1
   KMAX2=KMAX+2
   AK=KL
   SIGT(1)=SIGC*TKNST
   SIGT(2)=SIGC/ELAST
   SIGC(1)=SIGC*CHAR/ELAST
   SIGC(2)=SIGC*TKN**3/CHAR
   IF (IBC INL.LT.0) GO TO 14
   DO 58 I=1,4
   DO 58 J=1,4
   KKLM=J/4+1
   OMEGL(I,J)=OMEG1(I,J)*SIGT(KKLM)
   CAPLL(I,J)=CAPL1(I,J)*SIGC(KKLM)
   IF (IBCFNL.LT.0) GO TO 17
   DO 59 I=1,4
   DO 59 J=1,4
   KKLM=J/4+1
   OMEGL(I,J)=OMEG1(I,J)*SIGT(KKLM)
   CAPLL(I,J)=CAPL1(I,J)*SIGC(KKLM)
   LAM=TKN/CHAR
   SCE=.5*SCE
   DI=1.0-NU
   SI=1.0+NU
   LAM2=LAM**2
   IF (NDIMEN.LT.1) GO TO 228
   SIGC=1.0
   ELAST=1.0
   TKN=1.0
   CC 230 N=1,MAXM
   PFX(M)=C.0
   PFT(M)=0.0
   N(M)=0.0
   PX(M)=0.0
   PT(M)=0.0
   PR(M)=0.0
   TT(M)=0.0
   WT(M)=0.0

```


SAT07590
SAT08000
SAT08010
SAT08020
SAT08030
SAT08040
SAT08050
SAT08060
SAT08070
SAT08080
SAT08090
SAT08100
SAT08110
SAT08120
SAT08130
SAT08140
SAT08150
SAT08160
SAT08170
SAT08180
SAT08190
SAT08200
SAT08210
SAT08220
SAT08230
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SAT08250
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SAT08280
SAT08290
SAT08300
SAT08310
SAT08320
SAT08330
SAT08340
SAT08350
SAT08360
SAT08370
SAT08380
SAT08390
SAT08400
SAT08410
SAT08420
SAT08430
SAT08440
SAT08450
SAT08460

```

CT(M)=0.0
DMT(M)=C.0
MAXC(M)=0
MAXS(M)=0
MAXSY(M)=0
CALL GECM
ICFCK1=IABS(IGAMMA)+IABS(IOMEGS)+IABS(IOMEGT)+IABS(ICEOMS)
1 IC-CK2=IABS(IRADI)
  IF (.NOT. $PLOTS) GO TO 1001
  IC-CK2=IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(ICDSTF)
  IF (.NOT. $PLOTS) GO TO 1001
2 XSTATN(K)=FLQAT(K)
  IF (ICCHK1.EQ.0) GC TO 1001
  CC 1 K=1,KMAX
  XRADII(K)=R(K)*CHAR
  YGAMMA(K)=GAM(K)/CHAR
  YCMEGS(K)=OMXI(K)/CHAR
  YCMEGT(K)=CMT(K)/CHAR
  YCECMS(K)=DEOMX(K)/(CHAR*CHAR)
  CCNTINUE
10C1 CCNTINUE
8C4 WRITE(6,810)
  TEEC=TEEC
  IF (NDIMEN.EQ.1) TEEC=1.0
  CC 579 K=1,KMAX
  RKK=R(K)*CHAR
  CMXIK=CMXI(K)/CHAR
  GAMK=GAM(K)/CHAR
  CMTK=CMT(K)/CHAR
  DECMXK=DEOMX(K)/(CHAR*CHAR)
  AMSS=MASS(K)*TEED*2*ELAST*TKN/CHAR**2
97C WRITE(6,813) K,RKK,GAMK,CMXIK,CMTK,DECMXK,AMSS
8C5 MC=0
  M1=0
  M2=0
  M3=0
  AEN=CHAR/SIGO/TKN
  ZN=SIGC*TKN
  WRITE(6,112)
  CC 888 K=1,KMAX
  CALL BDE(K,B,DB,D,CC)
  EST=ELAST*TKN
  ZST=ELAST*TKN**3
  B=B*BST
  C=C*ZST
  CC=CB/CHAR*BST
  CC=DD/CHAR*ZST
  WRITE (6,71) K,B,C,CB,DC

```


IF (.NOT. \$PLOTS.OR. (ICHECK2.EQ.0)) GC TO 888

SAT08470
SAT08480
SAT08490
SAT08500
SAT08510
SAT08520
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SAT08540
SAT08550
SAT08560
SAT08570
SAT08580
SAT08590
SAT08600
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SAT08640
SAT08650
SAT08660
SAT08670
SAT08680
SAT08690
SAT08700
SAT08710
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SAT08730
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SAT08770
SAT08780
SAT08790
SAT08800
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SAT08840
SAT08850
SAT08860
SAT08870
SAT08880
SAT08890
SAT08900
SAT08910
SAT08920
SAT08930
SAT08940

```

888 IF (.NOT. $PLOTS.OR. (ICHECK2.EQ.0)) GC TO 888
    YES IF(K)=8
    YCSTIF(K)=C
    YRBSTIF(K)=DB
    YCCSTIF(K)=CC
    CCNTINUE
    CALL FLCAD(1,Z)
    CALL TLCAD(1,Z)
    CELSQ=CEL#2
    TCLI=.5/DEL
    TCEL=2.C*DEL
    MNINIT=1
    MNMAXC=MNMAX
    DC 20 I=1,4
    DC 20 J=1,4
    UNIT(I,J)=0.0
    IF(I.EQ.J) UNIT(I,J)=1.0
    NMAX=MAXM*KMAX2
    CC 22 K=1,NMAX
    DC 22 I=1,4
    ZCCT(I,K)=0.0
    ZC(I,K)=0.0
    Z2(I,K)=0.0
    Z3(I,K)=0.0
    Z(I,K)=0.0
    IF(IC.EC.0) GO TO 834
    CALL INITL(Z,Z0,Z2,Z3,ZCOT)
    ACC=CHAR*SIGC/ELAST
    ACM=SIGC*TKN**3/CHAR
    DC 830 M=1,MNMAX
    MN=(M-1)*KMAX2
    WRITE(6,126) N(M)
    WRITE(6,127)
    DO 831 K=2,KMAX1
    MK=K+MM
    TL=ACQ*ZO(1,MK)
    TV=ACQ*ZO(2,MK)
    TW=ACQ*ZO(3,MK)
    TM=ACM*ZC(4,MK)
    KK=K-1
    WRITE(6,71) KK,TU,TV,TW,TM
    WRITE(6,125)
    CC 830 K=2,KMAX1
    ACC=CHAR*SIGC/(ELAST*TEEO)
    AMC=SIGC*TKN**3/(CHAR*TEEO)
    MK=K+MM
    TL=ACD*ZDOT(1,MK)
    TV=ACD*ZDOT(2,MK)

```



```

      TW=ACD*ZDOT(3,MK)
      TM=AMD*ZDOT(4,MK)
      KK=K-1
      WRITE(6,71) KK,TU,TV,TH,TM
      CC 830 I=1,4
      Z(I,MK)=ZC(I,MK)+ZCCT(I,MK)*DELCAC
      Z2(I,MK)=ZC(I,MK)-ZDOT(I,MK)*DELCAC
      Z3(I,MK)=ZC(I,MK)-2.*ZDOT(I,MK)*DELCAD
      CCNTINUE
      ALCAD=1.0
      CALL IMPERF (PHIXB,PHITB)
      CALL FMATRIX (P,X,ZC,Z2,Z3,DEE,DST)
      LSTEP=1
      LCFANG=C
      ITR=1
      ICCRFL=0
      IF(MNMAX.EQ.MAXM) ICORFL=1
      IPASS=0
      ITTEST=0
400  CALL XANDZ (P,DEE,DST,X,Z,ZC,Z2,Z3,ZDOT,IS,JS,IC,JD,PHIXB,PHITB)
      IF(ITRMAX.EQ.1) GO TO 50
      MNMAXC=MNMAX
      IF(IPASS.LT.2) CALL MCODES (IS,JS,IC,JD,P,X,ZC,Z2,Z3,CEE,CST)
      IF(NCCNV.EQ.1) GO TO 50
      IF(ITR.LT.ITRMAX) GC TO 23
      GC TO 365
50  FL=LSTEP
      FI=IPRINT
      LI=LSTEP/IPRINT
      FLI=LI
      FI=FLI-FL/FI
      IF(FLI.EQ.0.) CALL OUTPUT(IMODE,P,CEE,DST,X,Z,ZC,Z2,Z3,ZCOT,IS,JS,
1  IF(JD,PHIXB,PHITB)
      IF(LSTEP.GE.LSMAX) GC TC 360
      CC 65 MN=1,MNMAX0
      DC 65 K=1,KMAX2
      IK=K+(MN-1)*KMAX2
      DC 65 I=1,4
      ZN=3.0*(Z(I,IK)-ZC(I,IK))+Z2(I,IK)
      Z3(I,IK)=Z2(I,IK)
      Z2(I,IK)=ZC(I,IK)
      ZC(I,IK)=ZN
      Z(I,IK)=ZN
      ALCAD=1.0
      LSTEP=LSTEP+1
      ITR=1
      GC TO 400
      ITR=ITR+1
23

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SAT08950
 SAT08960
 SAT08970
 SAT08980
 SAT08990
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 SAT09380
 SAT09390
 SAT09400
 SAT09410
 SAT09420
 SAT09430
 SAT09440


```

C** RCUND MAXIMUM TO NEXT HIGHEST 2 SIG FIGS *****
C** XMAX=AMAX1(0.,XMAX) *****
C** CALL RCUND(XMAX,IMX,FMX) *****
C** IMX=IMX-1 *****
C** FMX=FMX*10. *****
3 XMAX=FMX*10. ***** GC TO 2
C** IF(XMX.GE.XMAX) *****
C** FMX=FMX+1. *****
C** FMX=FMX *****
C** FMX=IMM *****
C** GC TO 3 *****
C** RCUND MINIMUM TO NEXT LOWEST 2 SIG FIGS *****
C** XMIN=AMIN1(0.,XMIN) *****
2 CALL RCUND(XMIN,IMN,FMN) *****
C** IMN=IMN-1 *****
14 XMIN=FMN*10. ***** GC TO 11
C** IF(XMIN.GE.XMN) *****
C** FMN=FMN-1. *****
C** FMN=FMN *****
C** FMN=IMM *****
C** GC TO 14 *****
C** RCUND MAX & MIN TC 1. OR .1 IF RANGE LARGE *****
C** *****
C** 11 XSC=XMX-XMN *****
C** IN=C *****
C** SA=1. *****
5 IF(XSC/CIV.LE.SM) GC TO 12 *****
C** IF(ABS(XMN).LT.SM.AND.ABS(XMN).GT.0.) XMN=SIGN(SM,XMN) *****
C** IF(ABS(XMX).LT.SM.AND.ABS(XMX).GT.0.) XMX=SIGN(SM,XMX) *****
12 IF(IM.GT.0) GO TO 19 *****
C** SM=1 *****
C** IN=IM+1 *****
C** GC TO 9 *****
C** RCUND RANGE (MAX-MIN) TC 2 SIG FIGS *****
C** *****
15 XSC=XMX-XMN *****
C** CALL RCUND(XSC,ISIC,FACTX) *****
C** *****
C** FINE FACTOR WHICH IS MULTIPLE OF IDIV *****
C** FACTX=FACTX*10. *****
C** CFAC=FACTX *****

```



```

1C CCATTINUE
1E FACT=FACT*10.**(-IDD)
IS=IS+IDD
C *****
C RCLND MANTISSA TO 2 SIG FIGS
C *****
C IFAC=FACT*10.+0.05
FACT=IFAC
FACT=FACT/10.
IF(FACT.LT.10.) GC TO 20
C *****
C SET TO 1 IF LESS THAN 10.
C *****
FACT=1.
IS=IS+1
C *****
C IF INPUT NEGATIVE, SET MANTISSA NEGATIVE
C *****
2C IF(ANUM.LT.0.) FACT=-FACT
RETURN
C *****
C SET TO C. IF 0.
C *****
1F FACT=0.
IS=C
RETURN
END
C *****
SUBROUTINE DRAWIT(X,Y,NCATA,RANGE,KKZ,MODCUR)
DIMENSION GRID(61,81),XSCALE(5),YSCALE(7)
DIMENSION X(1),Y(1),RANGE(4)
INTEGER*2 GRID,BLANK,CCT,XCHAR(4)/1H+,1H.,1H-,1H-,1HX/
NCATA=NCATA*KKZ
IF(MODCUR.GT.1) GC TO 444
C *****
C GRID IS THE MATRIX USED TO PLOT THE POINTS
C *****
IERR=0
XMAX=RANGE(1)
XMIN=RANGE(2)
YMAX=RANGE(3)
YMIN=RANGE(4)
C *****
C CHECKING X AND Y PCINTS AND PLOTTING THOSE CUT OF RANGE
C *****
C AT THE MARGIN
C *****
CC 30 I=1,KCATA,KKZ

```

SAT111370
SAT111380
SAT111390
SAT111400
SAT111410
SAT111420
SAT111430
SAT111440
SAT111450
SAT111460
SAT111470
SAT111480
SAT111490
SAT111500
SAT111510
SAT111520
SAT111530
SAT111540
SAT111550
SAT111560
SAT111570
SAT111580
SAT111590
SAT111600
SAT111610
SAT111620
SAT111630
SAT111640
SAT111650
SAT111660
SAT111670
SAT111680
SAT111690
SAT111700
SAT111710
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SAT111740
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SAT111770
SAT111780
SAT111790
SAT111800
SAT111810
SAT111820
SAT111830
SAT111840


```

      IF(X(I).GT.XMAX.OR.X(I).LT.XMIN.CR.Y(I).GT.YMAX.OR.Y(I).LT.YMIN)
      1 IERR=IERR+1
      IF(X(I).LE.XMAX) GC TC 205
      X(I)=XMAX
      GTC 21C
      205 IF(X(I).GE.XMIN) GO TO 210
      X(I)=XMIN
      21C IF(Y(I).LE.YMAX) GO TO 215
      Y(I)=YMAX
      GTC 3C
      215 IF(Y(I).GE.YMIN) GO TO 30
      Y(I)=YMIN
      3C CCNTINUE
      *****
      C** PLCTTING X AND Y AXIS ! IF NECESSARY *****
      C** *****
      C** *****
      JERR=0
      XMAX=XMAX-XMIN
      YRANGE=YMAX-YMIN
      IF(YRANGE.NE.0.) GO TO 298
      IF(YMIN.EQ.0.) GO TC 889
      YMIN=0.
      YRANGE=YMAX
      YRANGE=0.
      258 GC TO 259
      IF(XRANGE.NE.0.) GO TO 295
      IF(XMIN.EQ.0.) GO TC 887
      XMIN=0.
      XRANGE=XMAX
      *****
      C** BLANKING CUT MATRIX-(GRID) *****
      C** *****
      C** *****
      255 CC 300 I=1,61
      CC 301 JJ=1,81
      301 GRCT(I,JJ)=BLANK
      CCNTINUE
      IF(XMAX*XMIN.GE.0.) GO TO 222
      IYAXIS=80.*(-XMIN)/XRANGE+1.5
      CC 40 I=1,61
      40 GRCT(I,IYAXIS)=DOT
      222 IF(YMAX*YMIN.GE.0.) GO TO 333
      IXAXIS=60.*YMAX/YRANGE+1.5
      CC 60 I=1,81
      6C GRCT(IXAXIS,I)=DOT
      *****
      C** COMPUTE PROPER SCALE NUMBERS *****
      C** *****
      C** *****
      323 XINCR=XRANGE/4.
      YINCR=YRANGE/6.

```



```

1 YDEQMS(200),YBSTIF(200),YCSITF(200),YBSTF(200),YBSTF(200),
2 YDDSTF(200),YPR(200),YPS(200),YPT(200),YPT(200),YPT(200),
3 YMT(200),YDTT(200),YDMT(200),YNS(200),YNTF(200),
4 YNSTH(200),YQS(200),YMS(200),YMT(200),YNSTH(200),
5 YU(200),YV(200),YW(200),YPTIS(200),YPTIT(200),
6 YPHI(200),XSTATN(200)
DIMENSION PTF(500),PF(500)
*****
AEZC=SIGO/ELAST
1 IF($DYAMC) GO TO 181
WRITE(6,101) LSTEP,ALOAD,ITR
GC TO 182
181 TTI=LSTEP*DELOAD
TTI=TTI*TEEC
WRITE(6,151) LSTEP,TTI,DTI,ITR
182 LAM=TKN/CHAR
ENL=1
AEZ=SIGC*TKN
AEZ3=ABZ*TKN*TKN/CHAR
AEZN=CHAR*SIGO/ELAST
IF(ITRM*AX.EQ.1) ENL=0.
CC2=1.-NU*2
C2I=1./CD2
CPI=1./SI
CNI=1./CI
TCLSQI=.5/DELSQ
1 ICHK1=IABS(INTH)+IABS(INSTH)+IABS(IQS)+IABS(IMS)
1 ICHK2=IABS(IU)+IABS(IV)+IABS(IW)+IABS(IPHIS)+IABS(IPHIT)
1 IF(NT+MAX.EQ.0) GC TO 991
DC 21 NTH=1,NTHMAX
DC 1 MN=1,MNMAX
1 I1=1+(MN-1)*KMAX2
I2=I1+1
U1(MN)=Z(1,I1)
U2(MN)=Z(1,I2)
V1(MN)=Z(2,I1)
V2(MN)=Z(2,I2)
W1(MN)=Z(3,I1)
W2(MN)=Z(3,I2)
1 TRET=TF(NT)
WRITE(6,116) THET
DC 121 K=1,KMAX
K1=K+1
CALL BCB(K,BS,DB,CS,DD)
IF(K.EQ.1.AND.IBCINL.LT.0) CALL PCLE(K,P,DEE,CST,X,Z,ZO,Z2,Z3,
1 ZDCT,IS,JS,ID,JD,PHIXB,PHITE)

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IF(K-EQ-1.AND.IBCINL.LT.O) GO TC 595
IF(K-EQ.KMAX.AND.IBCFNL.LT.O) CALL POLE(K,P,CEE,DST,X,Z,ZO,Z2,Z3,
1ZCCT,IS,JS,JD,PHIXB,PHITB)
IF(K-EQ.KMAX.AND.IBCFNL.LT.O) GO TO 999
CALL PHIBET(K,Z,IS,JS,JD,PHIXB,PHITB)
CEX=DECMX(K)
FRA=1./R(K)
CX=CMXI(K)
CT=CMT(K)
GA=CAM(K)
DCXT=GX-CT
CCC=GA*COXT
CC2C=CC2*DS
CC 3 MN=1,MNMAXQ
EN=N(MN)
ENR=EN*FRA
CALL TLOAD(K,Z)
TTS=TT(MN)*ALOAD
EX=(U3(MN)-U1(MN))*TDLI+OX*W2(MN)+ENL*OSE*(BX3(MN)+BE3(MN))
ET=ENR*V2(MN)+GA*U2(MN)+OT*W2(MN)+ENL*OSE*(BT3(MN)+BE3(MN))
EXT=.5*((V3(MN)-V1(MN))*TDLI-ENR*U2(MN)-GA*V2(MN)+ENL*SCE*BXT3(MN)
1)
KT=ENR*PHIT(MN)+GA*PHIX(MN)
KXT=.5*(ENR*(-PHIX(MN)-GA*W2(MN)+(W3(MN)-W1(MN))*TDLI)+GCO*V2(MN)
+OT*(V3(MN)-V1(MN))*TDLI-GA*PHIT(MN)-CCXT*PHI(MN))
TX(MN)=ES*(EX+NU*ET)-TTS
TTH(MN)=BS*(ET+NU*EX)-TTS
TXI(MN)=BS*D1*EXT
MKI=KI+(MN-1)*KMAX2
MX(MN)=Z(4,MKI)
MTF(MN)=NU*MX(MN)+DC2D*KT-D1*MT(MN)*ALOAD
XT(MN)=DS*D1*KXT
MKI1=MKI+1
MKKI=MKI-1
CS(MN)=SIGO*TKN*LAM2*(GA*MX(MN)+(Z(4,MKI1)-Z(4,MKKI1))*TDLI
+ENR*MX(MN)-GA*TH(MN))
1 MX(MN)=MX(MN)*ABZ3
MTF(MN)=MTH(MN)*ABZ3
XT(MN)=MXT(MN)*ABZ3
TX(MN)=TX(MN)*ABZ
TTH(MN)=TTH(MN)*ABZ
TXI(MN)=TXI(MN)*ABZ
PHIX(MN)=PHIX(MN)*ABZQ
PHIT(MN)=PHIT(MN)*ABZC
PFI(MN)=PFI(MN)*ABZO
L1(MN)=L1(MN)
L2(MN)=L2(MN)
V1(MN)=V2(MN)
SAT114250
SAT114260
SAT114270
SAT114280
SAT114290
SAT114300
SAT114310
SAT114320
SAT114330
SAT114340
SAT114350
SAT114360
SAT114370
SAT114380
SAT114390
SAT114400
SAT114410
SAT114420
SAT114430
SAT114440
SAT114450
SAT114460
SAT114470
SAT114480
SAT114490
SAT114500
SAT114510
SAT114520
SAT114530
SAT114540
SAT114550
SAT114560
SAT114570
SAT114580
SAT114590
SAT114600
SAT114610
SAT114620
SAT114630
SAT114640
SAT114650
SAT114660
SAT114670
SAT114680
SAT114690
SAT114700
SAT114710
SAT114720

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V2(MN)=V3(MN)
W1(MN)=W2(MN)
W2(MN)=W3(MN)
FK=K-1
FIFREQ=IFREQ
FK1ST=(K-1)/IFREQ
FK1ST=K1ST
FKTEST=FK/FIFREQ-FK1ST
IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 999
IF(FKTEST.NE.0.) GO TO 2
555 X(1,K)=C.
X(2,K)=C.
X(3,K)=0.
X(4,K)=C.
PTF(K)=C.
PF(K)=0.
ANX=0.
ANXF=0.
ANXTH=0.
ANX=0.
ANXF=0.
ANXTH=0.
ANXTH=0.
AGS=0.
IF(JUMP.EQ.2) GO TO 73
DC 72 MN=1,MNMAXO
EN=N(MN)
FC=EN*THET
CS=SIN(FC)
CS=cos(FC)
X(1,K)=X(1,K)+U1(MN)*CS*ABZN
X(2,K)=X(2,K)+V1(MN)*SN*ABZN
X(3,K)=X(3,K)+W1(MN)*CS*ABZN
X(4,K)=X(4,K)+PHIX(MN)*CS
PTF(K)=PTF(K)+PHIT(MN)*SN
ANX=ANX+MX(MN)*CS
ANXF=AMTH+MTH(MN)*CS
ANXTH=ANXF+MX(MN)*SN
ANX=ANX+IX(MN)*CS
ANXF=ANXF+TTH(MN)*CS
AGS=AGS+QS(MN)*CS
ANXTH=ANXTH+TX(MN)*SN
PF(K)=PF(K)+PHI(MN)*SN
72 ***
C***
GC 72 429
73 CC 74 MN=3,MNMAXO,JUMP
EN=N(MN)
FC=EN*THET
SN=SIN(FC)
SAT114730
SAT114740
SAT114750
SAT114760
SAT114770
SAT114780
SAT114790
SAT114800
SAT114810
SAT114820
SAT114830
SAT114840
SAT114850
SAT114860
SAT114870
SAT114880
SAT114890
SAT114900
SAT114910
SAT114920
SAT114930
SAT114940
SAT114950
SAT114960
SAT114970
SAT114980
SAT114990
SAT115000
SAT115010
SAT115020
SAT115030
SAT115040
SAT115050
SAT115060
SAT115070
SAT115080
SAT115090
SAT115100
SAT115110
SAT115120
SAT115130
SAT115140
SAT115150
SAT115160
SAT115170
SAT115180
SAT115190
SAT115200

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```

CS=CCS(FC)
MNM=MN-1
X(1,K)=X(1,K)+(U1(MN)*CS+U1(MNM)*SN)*ABZN
X(2,K)=X(2,K)+(V1(MN)*CS+V1(MNM)*CS)*ABZN
X(3,K)=X(3,K)+(W1(MN)*CS+W1(MNM)*SN)*ABZN
X(4,K)=X(4,K)+PHIX(MN)*CS+PHIX(MNM)*SN
PTF(K)=PTF(K)+PHIT(MN)*SN+PHIT(MNM)*CS
AMX=AMX+MX(MN)*CS+MX(MNM)*SN
AMTH=AMTH+MTH(MN)*CS+MTH(MNM)*SN
AMXT=AMXT+MX(MN)*CS+MX(MNM)*SN
ANX=ANX+TX(MN)*CS+TX(MNM)*SN
ANTH=ANTH+TTH(MN)*CS+TTH(MNM)*SN
ANXT=ANXT+TTH(MN)*CS+TTH(MNM)*SN
ACS=ACS+QS(MN)*CS+QS(MNM)*SN
PF(K)=PF(K)+PHI(MN)*CS+PHI(MNM)*CS
X(1,K)=X(1,K)+U1(1)*ABZN
X(2,K)=X(2,K)+V1(1)*ABZN
X(3,K)=X(3,K)+W1(1)*ABZN
X(4,K)=X(4,K)+PHIX(1)
PTF(K)=PTF(K)+PHIT(1)
PF(K)=PF(K)+PHI(1)
AMX=AMX+MX(1)
AMTH=AMTH+MTH(1)
AMXT=AMXT+MX(1)
ANX=ANX+TX(1)
ANTH=ANTH+TTH(1)
ANXT=ANXT+TTH(1)
ACS=ACS+QS(1)

```

74

C*****

```

CONTINUE
IF(K.EQ.1) WRITE(6,117)
WRITE(6,118) K,ANX,ANTH,ANXTH,AQS,AMX,AMTH,AMXTH
IF ($MOD(CAL.CR.(ICFCK1.EQ.0))) GO TO 2

```

121

```

YNS(K)=ANX
YNTF(K)=ANTH
YNSTH(K)=ANXTH
YCS(K)=AQS
YMS(K)=AMX
YMTF(K)=AMTH
YNSTH(K)=AMXTH
CONTINUE
CC 66C K=1,KMAX
FK=K-1
FIFREQ=IFREQ
FKTST=(K-1)/IFREQ
FKTST=K1ST
FKTEST=FK/FIFREQ-FKTST

```

SAT115210
SAT115220
SAT115230
SAT115240
SAT115250
SAT115260
SAT115270
SAT115280
SAT115290
SAT115300
SAT115310
SAT115320
SAT115330
SAT115340
SAT115350
SAT115360
SAT115370
SAT115380
SAT115390
SAT115400
SAT115410
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SAT115430
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SAT115490
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SAT115560
SAT115570
SAT115580
SAT115590
SAT115600
SAT115610
SAT115620
SAT115630
SAT115640
SAT115650
SAT115660
SAT115670
SAT115680


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661 IF (K.EC.1.OR.K.EQ.KMAX) GO TO 661
IF (FKTEST.NE.0.) GO TO 658
IF (K.EC.1) WRITE(6,217)
WRITE(6,218) K,X(1,K),X(2,K),X(3,K),X(4,K),FTF(K),PF(K)
IF ($MOCAL.OR.(ICFCK2.EQ.0)) GO TO 658
YL(K)=X(1,K)
YV(K)=X(2,K)
Yw(K)=X(3,K)
YPHIS(K)=X(4,K)
YPHIT(K)=PTF(K)
YFTI(K)=PF(K)
DC 659 I=1,4
X(I,K)=0.
CCNTINUE
IF ($PLCITS.AND..NOT.$MOCAL.AND.((ICCHK1.GT.0).OR.(ICFCK2.GT.0)))
1 CALL PLOT2(NTH)
21 CCNTINUE
LE.0) RETURN
DC 534 MN=1,MNMAXQ
WRITE(6,749) N(MN)
DC 521 MM=1,MNMAXC
I1=1+(MN-1)*KMAX2
I2=I1+1
U1(MM)=Z(1,I1)
U2(MM)=Z(1,I2)
V1(MM)=Z(2,I1)
V2(MM)=Z(2,I2)
W1(MM)=Z(3,I1)
W2(MM)=Z(3,I2)
CCNTINUE
DC 445 K=1, KMAX
K1=K+1
CALL BCCE(K,BS,DB,CS,DC)
IF (K.EQ.1.AND.IBCINL.LT.0) CALL PCLE(K,P,DEE,CST,X,Z,ZO,Z2,Z3,
1 ZCCT,IS,JS,ID,JD,PHIXB,PHITB)
IF (K.EQ.KMAX.AND.IBCFNL.LT.0) CALL POLE(K,P,DEE,DST,X,Z,ZO,Z2,Z3,
1 ZCCT,IS,JS,ID,JD,PHIXB,PHITB)
TXZ=TX(MN)
THZ=TH(MN)
TXTZ=TXT(MN)
AMXZ=MX(MN)
AMTHZ=MT(MN)
AMXTZ=MX(MN)
CSZ=QS(MN)
X(1,K)=PHIX(MN)
X(2,K)=PHIT(MN)
X(3,K)=PHI(MN)
IF (K.EQ.1.AND.IBCINL.LT.0) GO TO 583
SAT115690
SAT115700
SAT115710
SAT115720
SAT115730
SAT115740
SAT115750
SAT115760
SAT115770
SAT115780
SAT115790
SAT115800
SAT115810
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SAT115830
SAT115840
SAT115850
SAT115860
SAT115870
SAT115880
SAT115890
SAT115900
SAT115910
SAT115920
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SAT115940
SAT115950
SAT115960
SAT115970
SAT115980
SAT115990
SAT116000
SAT116010
SAT116020
SAT116030
SAT116040
SAT116050
SAT116060
SAT116070
SAT116080
SAT116090
SAT116100
SAT116110
SAT116120
SAT116130
SAT116140
SAT116150
SAT116160

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IF(K.EQ.KMAX.AND.IBCFNL.LT.0) GC TC 583
 CALL PHIBET(K,Z,IS,JS,JD,PHIXB,PHITB)

CEX=DECIM(K)
 RRA=1./R(K)
 CX=CMXI(K)
 CT=CMT(K)
 GA=GAM(K)
 CCXT=OX-CT
 GCC=GA*CCXT
 DL2D=CC2*DS
 ENR=EN*RRRA
 CALL TLCAD(K,Z)
 TTS=TT(MN)*ALOAD
 EX=(U3(MN)-U1(MN))*TDLI+OX*W2(MN)+ENL*OSE*(BX3(MN)+BE3(MN))
 ET=ENR*V2(MN)+GA*U2(MN)+OT*W2(MN)+ENL*OSE*(BT3(MN)+BE3(MN))
 EXT=.5*((V3(MN)-V1(MN))*TDLI-ENR*U2(MN)-GA*V2(MN)+ENL*SOE*BX12(MN))
 1) KT=ENR*PHIT(MN)+GA*PHIX(MN)
 KXT=.5*(ENR*(-PHIX(MN)-GA*W2(MN)+(W3(MN)-W1(MN))*TDLI)+GCC*V2(MN)
 1) +OT*(V3(MN)-V1(MN))*TDLI-GA*PHIT(MN)-CCXT*PHI(MN))
 TX2=(BS*(EX+NU*ET)-TTS)*ABZ
 THZ=(BS*(ET+NU*EX)-TTS)*ABZ
 TXIZ=BS*D1*EXT*ABZ
 WK1=K1+(MN-1)*KMAX2
 AMXZ=Z(4,MK1)
 AMTHZ=NU*AMXZ+DD2D*KT-DI*MT(MN)*ALCAD
 AMXIZ=CS*CI*KXT
 MK11=MK1+1
 MKK1=MK1-1
 CSZ=SIGD*TKN*LAM2*(GA*AMXZ+(Z(4,MK11)-Z(4,MKK1))*TDLI+ENR*AMXIZ
 1) -GA*AMTHZ)
 AMXZ=AMXZ*ABZ3
 AMTHZ=AMTHZ*ABZ3
 AMXIZ=AMXIZ*ABZ3
 X(1,K)=PHIX(MN)*ABZC
 X(2,K)=PHIT(MN)*ABZC
 X(3,K)=PHI(MN)*ABZC
 CC233=MM=1,MNMAXC
 L1(MN)=L2(MN)
 L2(MN)=U3(MN)
 V1(MN)=V2(MN)
 V2(MN)=V3(MN)
 W1(MN)=W2(MN)
 W2(MN)=W3(MN)
 FK=K-1
 FIFREQ=IFREQ
 KTST=(K-1)/IFREQ

533


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FKTST=K1ST
FKTEST=FK/FIFREQ-FK1ST
IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 583
IF(FKTEST.NE.0.) GC TO 445
583 CCNTINUE
IF(K.EQ.1) WRITE(6,117)
117 WRITE(6,118) K,TXZ,TTHZ,TXIZ,QSZ,AMXZ,AMT1Z,AMXIZ GC TC 445
IF(.NOT.$PLOTS.OR..NOT.$MODAL.CR.(ICHECK1.EC.0)) GC TC 445
YAS(K)=TXZ
YATF(K)=TTHZ
YASTH(K)=TXIZ
YCS(K)=CSZ
YMS(K)=AMXZ
YMTF(K)=AMTHZ
YMSTH(K)=AMXIZ
CCNTINUE
445 WRITE(6,217)
446 DC 447 K=1,KMAX
FK=K-1
FIFREQ=IFREQ
K1ST=(K-1)/IFREQ
FKTST=K1ST
FKTEST=FK/FIFREQ-FK1ST
IF(K.EQ.1.CR.K.EQ.KMAX) GO TO 593
IF(FKTEST.NE.0.) GO TO 447
593 KZ=K+1+(MN-1)*KMAX2
LP=Z(1,KZ)*ABZN
VP=Z(2,KZ)*ABZN
WP=Z(3,KZ)*ABZN
WRITE(6,218) K,UP,VP,WP,X(1,K),X(2,K),X(3,K)
IF(.NOT.$PLOTS.OR..NOT.$MODAL.CR.(ICHECK2.EC.0)) GC TC 447
YL(K)=UP
YV(K)=VP
YW(K)=WF
YFIS(K)=X(1,K)
YFIT(K)=X(2,K)
YFI(K)=X(3,K)
447 CCNTINUE
IF ($PLOTS.AND.$MODAL.AND.((ICHECK1.GT.0).OR.(ICHECK2.GT.0)))
1 CALL PLCT2(1)
534 CCNTINUE
C *****
101 FCRMAT(1,'',THE LCAC STEP NUMBER IS',I2,'
101 LCAC FACTOR IS',E11.4,'THE SOLUTION CONVERGED IN',I2,'
21 ITERATIONS,////)
116 FCRMAT(0,'',THE SUMMED FCRCES, MCMENTS, DISPLACEMENTS AN
117 FCRMAT('/',STATION FOLLOW FOR THETA ='E15.6//') N S N ST-ETA

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```

CCMCN /BL3/
CCMCN /BL4/
1 CCMCN /BL5/
CCMCN /BL6/
CCMCN /BL7/
CCMCN /BL8/
CCMCN /BL9/
CCMCN /BL14/
CCMCN /BL15/
1 CCMCN /BL16/
CCMCN /BL18/
CCMCN /BL27/
CCMCN /BL28/
CCMCN /BL29/
1 CCMCN /BL30/
1 CCMCN /BL31/
CCMCN /BL100/
CCMCN /BL101/
CCMCN /BL102/
CCMCN /BL103/
DIMENSION ELLS(4),CL1(4,4),CL2(4,4)
1,CL0(4,4),CL1(4,4),ZDD(4)
2,TZMAX(4,99),ZDD(4)
EQCIVALANCE (CL0(1),ZFIM(1)),(CL1(1),ZF2M(1)),(CL2(1),ZF3M(1))
*****
CC 201 I=1,4
CC 201 M=1,MNMAX
TJ=1+(M-1)*KMAX2
TZMAX(I,M)=ABS(Z(I,MJ))
CC 201 K=2,KMAX2
KF=K+(M-1)*KMAX2
AZTST=ABS(Z(I,KM))
IF(AZTST.GT.TZMAX(I,M)) TZMAX(I,M)=AZTST
2C1
NCCNV=1
IF(ITRMX.EQ.1) GC TC 66
DC 1 M=1,MNMAXO
I=1+(KMXX+2)*(M-1)
U1(M)=Z(1,I)
V1(M)=Z(2,I)
W1(M)=Z(3,I)
I1=I+1
U2(M)=Z(1,I1)
V2(M)=Z(2,I1)
SAT17610
PR(99),PX(99),PT(99)
ZF1M(4,4,99),ZF2M(4,4,99),
ZF3M(4,4,99),ZF4M(4,4,99)
TT(99),MT(99),DT(99),DMT(99)
SOE,CSE,ALOAD
DI(500),GAM(500),OMT(500)
FFS(4,99),ELIS(4),GEES(4,99)
LAM2,LSO18,LSO1N
NU,U1(99),V1(99),W1(99),V2(99),U2(99),W2(99),U3(99),
V3(99),W3(99)
EPS
EL1(4),ELL(4),BXT3(99),BE3(99)
EXX3(99),ETT3(99),ETX3(99),EX2(99),ET3(99)
BXT1(99),BT1(99),BXT1(99),BE1(99),BX2(99),BT2(99),
BXT2(99),BE2(99)
EXX1(99),ETT1(99),ETX1(99),EX1(99),ET1(99),EXX2(99),
ETT2(99),ETX2(99),EXT2(99),ET2(99)
DELSQ,EXT1(99)
TEEC,$DYNMC
DELSO
DELOAD
MASS(500)
FLS(4),ZI(4),IPIVOT(4),INDEX(4,2)
CL2(4,4)
SAT17640
SAT17650
SAT17660
SAT17670
SAT17690
SAT17700
SAT17710
SAT17720
SAT17730
SAT17740
SAT17750
SAT17760
SAT17770
SAT17780
SAT17790
SAT17800
SAT17810
SAT17820
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SAT17920
SAT17930
SAT17940
SAT17950
SAT17960
SAT17970
SAT17980
SAT17990
SAT18000
SAT18010
SAT18020
SAT18030
SAT18040
SAT18050
SAT18060
SAT18070
SAT18080

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1  W2(M)=Z(3,I1)
   IF(IBCINL.LT.0) GC TO 100
   CALL PHIBET(1,Z,IS,JS,ID,JD,PHIXB,PHITB)
   CC 2 N=1,MNMAX
   BXT1(M)=BX3(M)
   BXT1(M)=BT3(M)
   BXT1(M)=BX3(M)
   BE1(M)=BE3(M)
   CALL TEAETA(1,Z,IS,JS,ID,JD)
   CC 3 M=1,MNMAX
   EXX1(M)=EXX3(M)
   ETT1(M)=ETT3(M)
   ETT1(M)=ETT3(M)
   EXX1(M)=EXX3(M)
   ETT1(M)=ETT3(M)
   CALL PHIBET(2,Z,IS,JS,ID,JD,PHIXB,PHITB)
   CC 4 N=1,MNMAX
   BX2(M)=BX3(M)
   BX2(M)=BT3(M)
   BX2(M)=BX3(M)
   BE2(M)=BE3(M)
   CALL TEAETA(2,Z,IS,JS,ID,JD)
   CC 5 N=1,MNMAX
   EXX2(M)=EXX3(M)
   ETT2(M)=ETT3(M)
   ETT2(M)=ETT3(M)
   EXX2(M)=EXX3(M)
   ETT2(M)=ETT3(M)
   CALL PHIBET(3,Z,IS,JS,ID,JD,PHIXB,PHITB)
   CCNT INUE
   IF(IBCINL.LT.0) GC TO 20
   CALL BOB(1,B1,DB,D,CD)
   GAM1=GAM(1)
   CALL TLCCAD(1,Z)
   CC 8 N=1,MNMAX
   IF(ITRMAX.EQ.1) GO TO 67
   FFS(1,M)=-TT(M)*ALCAD+OSE*(BX1(M)+BE1(M)+NU*(BT1(M)+BE1(M)))*B1
   FFS(2,M)=OSE*(B1*CI*EXT1(M)+EX1(M))
   FFS(3,M)=LAM2*GAM1*DI*MT(M)*ALOAD-(EXX1(M)+ETX1(M))*SOE
   GC TO 8
   FFS(1,M)=-TT(M)*ALCAD
   FFS(2,M)=0
   FFS(3,M)=LAM2*GAM1*DI*MT(M)*ALOAD
   FFS(4,M)=0
   CC 9 I=1,4

```



```

5  ELIS(I)=ALOAD*ELI(I)
20 CALL FORCE(1,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CALL FCRCE(2,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CC 10 K=3,KLL
   KF=K+1
   IF(ITRMAX.EQ.1) GO TO 1C
   CALL UPDATE
   CALL PHIBET(KP,Z,IS,JS,ID,JD,PHIXE,PHITB)
   CALL TEAETA(KP,Z,IS,JS,ID,JD)
   CALL FCRCE(K,P,X,DEE,DST,Z,ZO,Z2,Z3)
1C  IF(ITRMAX.NE.1) CALL UPDATE
   IF(IBCFL.LT.0) GO TO 120
   IF(ITRMAX.EQ.1) GO TO 11
   CALL PHIBET(KMAX,Z,IS,JS,ID,JD,PTIXB,PHITB)
   CALL TEAETA(KMAX,Z,IS,JS,ID,JD)
11  CALL FCRCE(KL,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CALL FORCE(KMAX,P,X,DEE,DST,Z,ZO,Z2,Z3)
12  CC 12 I=1,4
   ELIS(I)=ALOAD*ELI(I)
   GAML=BCE(KMAX,BL,DB,D,DD)
   FLS(4)=GAML(KMAX)
   CALL TLCD(KMAX,Z)
   CC 14 N=1,MKMAX
   IF(M.GT.1) ELLS(1)=0.0
   IF(ITRMAX.EQ.1) GC TO 68
   FLS(1)=-TT(M)*ALCAC+QSE*(BX3(M)+BE3(M)+NU*(ET3(M)+BE3(M)))*BL
   FLS(2) =QSE*(BL*CI*BXT3(M)+EX3(M)+ET3(M))
   FLS(3) =LAM2*GAML*CI*MT(M)*ALOAD-(EXX3(M)+ETX3(M))*SOE
   GC TO 65
68  FLS(1)=-TT(M)*ALOAD
   FLS(2)=C
   FLS(3)=LAM2*GAML*D1*MT(M)*ALOAD
69  CC CONTINUE
   IK=KL+KMAX*(M-1)
   IJ=KMAX*M
   L=N*KMAX2
   CC 14 I=1,4
   SUMZ=0.
   CC 15 J=1,4
   C*****
   C THE FOLLOWING CARD CAUSES BCUNDARY CONS TO EXIST FCR MODE 'O' ONLY
   C*****
   IF (M.NE.1) ELLS(J)=0
15  SUMZ=SUMZ+ZF1M(I,J,M)*ELLS(J)+ZF2M(I,J,M)*X(J,IJ)+ZF3M(I,J,M)*
14  X(J,IK)+ZF4M(I,J,M)*FLS(J)
   L=L+1

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SAT18570
SAT18600
SAT18610
SAT18620
SAT18630
SAT18640
SAT18650
SAT18670
SAT18680
SAT18690
SAT18700
SAT18710
SAT18740
SAT18750
SAT18760
SAT18770
SAT18780
SAT18790
SAT18800
SAT18810
SAT18820
SAT18830
SAT18840
SAT18850
SAT18860
SAT18870
SAT18880
SAT18890
SAT18900
SAT18910
SAT18920
SAT18930
SAT18940
SAT18950
SAT18960
SAT18970
SAT18980
SAT18990
SAT19000
SAT19010
SAT19020
SAT19030
SAT19040

```



```

150 CC 16 N=1,MNMAX
CC 16 L=L3,KMAX
K=KMAX2-L
KFX=K-1
KZ=K+1
IJ=KFX+(M-1)*KMAX
JK=KZ+(N-1)*KMAX2
KK=JK-1
CC 17 I=1,4
SUMZ=0.
CC 18 J=1,4
SUMZ=SUMZ-P(I,J,IJ)*Z(J,JK)
SUMZ=SUMZ+X(I,I,IJ)
ASUMZ=ABS(SUMZ)
IF(ASUMZ.GT.1.E+15) ITR=ITRMAX
IF(NCCNV.NE.1.OR.ASUMZ.LT.1.E-05) GO TC 17
DELZ=ABS(Z(I,KK)-SUMZ)
ZTEST=EFS*TZMAX(I,M)
IF(DELZ.GT.ZTEST) NCONV=0
Z(I,KK)=SUMZ
CC 17 CONTINUE
16 IF(IBCINL.LT.0) GO TO 30
CC 25 M=1,MNMAX
CALL EFG(I,M,ZO,Z2,Z3)
CALL ABC
IJ=2+(N-1)*KMAX2
1.1=IJ+1
1.2=IJ-1
CC 21 I=1,4
SUMZ=0.
CC 22 J=1,4
SUMZ=SUMZ-A(I,J)*Z(J,IJ1)-BEE(I,J)*Z(J,IJ)
Z(I,I)=SUMZ+GEES(I,M)
CC 21 MATINV(C,4,Z1,1,DETERM,IPIVOT,INDEX,4,ISCALE)
CC 23 I=1,4
Z(I,IJ2)=Z(I,I)
CC 23 CONTINUE
CC 23 RETURN
CALL INLPOL(Z,PHIXB,PHITB)
CC 101 M=1,MNMAX
L1(M)=U2(M)
V1(M)=V2(M)
W1(M)=W2(M)
I2=3+KMAX2*(M-1)
L2(M)=Z(1,IJ)
V2(M)=Z(2,IJ)
W2(M)=Z(3,IJ)
101 GC TO 102

```

SAT119050
SAT119060
SAT119070
SAT119080
SAT119090
SAT119100
SAT119110
SAT119120
SAT119130
SAT119140
SAT119150
SAT119160
SAT119170
SAT119180
SAT119190
SAT119200
SAT119210
SAT119220
SAT119230
SAT119240
SAT119250
SAT119260
SAT119270
SAT119280
SAT119290

SAT119310
SAT119320
SAT119330
SAT119340
SAT119350
SAT119360
SAT119370
SAT119380
SAT119390
SAT119400
SAT119410
SAT119420
SAT119430
SAT119440
SAT119450
SAT119460
SAT119470
SAT119480
SAT119490
SAT119500
SAT119510
SAT119520


```

120 IF(ITRMAX.NE.1) CALL FNLPOL (Z,P,PIXB,PHITB)
    CALL FCRCE(KL,P,X,DEE,DST,Z,ZC,Z2,Z3)
    IF(M2.EC.0) GO TO 122
    L=KL+(M2-1)*KMAX
    LI=KMAX1+(M2-1)*KMAX2
    CC 130 I=1,4
    SUM=0.
    CC 131 J=1,4
    SUM=SUM+CL2(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF(NCONV.NE.1.OR.ASUMZ.LT.1.E-05) GO TC 130
    CELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*TZMAX(I,M2)
    IF(CELZ.GT.ZTEST) NCONV=0
    130 IF(I,L1)=SUM
    122 IF(M1.EC.0) GO TO 123
    L=KL+(M1-1)*KMAX
    LI=KMAX1+(M1-1)*KMAX2
    CC 132 I=1,4
    SUM=0.
    CC 133 J=1,4
    SUM=SUM+CL1(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF(NCONV.NE.1.OR.ASUMZ.LT.1.E-05) GO TC 132
    CELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*TZMAX(I,M1)
    IF(CELZ.GT.ZTEST) NCONV=0
    132 IF(I,L1)=SUM
    123 IF(M0.EC.0) GO TO 124
    L=KL+(M0-1)*KMAX
    LI=KMAX1+(M0-1)*KMAX2
    CC 134 I=1,4
    SUM=0.
    CC 135 J=1,4
    SUM=SUM+CLC(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF(NCONV.NE.1.OR.ASUMZ.LT.1.E-06) GO TC 134
    CELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*TZMAX(I,M0)
    IF(CELZ.GT.ZTEST) NCONV=0
    134 IF(I,L1)=SUM
    124 ZC=2
    GC TO 150
    ENC

SLEROUTINE PLOT2(NTN)
*****
C THIS SUBROUTINE CALLS PLOTTING ROUTINES FOR APPROPRIATE (USER
*****
SAT119530
SAT119550
SAT119560
SAT119570
SAT119580
SAT119590
SAT119600
SAT119610
SAT119620
SAT119630
SAT119640
SAT119650
SAT119660
SAT119670
SAT119680
SAT119690
SAT119700
SAT119710
SAT119720
SAT119730
SAT119740
SAT119750
SAT119760
SAT119770
SAT119780
SAT119790
SAT119800
SAT119810
SAT119820
SAT119830
SAT119840
SAT119850
SAT119860
SAT119870
SAT119880
SAT119890
SAT119900
SAT119910
SAT119920
SAT119930
SAT119940
SAT119950
SAT119960
SAT119970
SAT119980
SAT119990
*****
SAT20000

```



```

C ***** SPECIFIED) CPUTPUT QUANTITIES *****
C ***** IAPFLICIT LCGICAL*1 ($) *****
C ***** CCMCMCN /IBL4/ KMAX,KL *****
C ***** CCMCMCN /BL19/ TH(36) *****
C ***** CCMCMCN /BLPLOT/ *****
C ***** 1 2 3 *****
C ***** CCMCMCN /BLPLTL/ *****
C ***** 1 2 3 4 5 6 *****
C ***** NGKMAX=-KMAX *****
C ***** IF ($MCCAL) GO TO 121 *****
C ***** IF (INS.EQ.0) GO TO 4 *****
C ***** WRITE (6,1000) *****
C ***** IF (INS.GT.0) CALL PLOTIT (XSTATN,YNS,KMAX,C) *****
C ***** IF (INS.LT.0) CALL PLOTIT (XSTATN,YNS,NGKMAX,0) *****
C ***** WRITE (6,1001) TH(NTH) *****
C ***** IF (INTF.EQ.0) GO TO 5 *****
C ***** WRITE (6,1000) *****
C ***** IF (INTF.GT.0) CALL PLOTIT (XSTATN,YNTH,KMAX,C) *****
C ***** IF (INTF.LT.0) CALL PLOTIT (XSTATN,YNTH,NGKMAX,0) *****
C ***** WRITE (6,1002) TH(NTH) *****
C ***** IF (INSTH.EQ.0) GO TO 6 *****
C ***** WRITE (6,1000) *****
C ***** IF (INSTH.GT.0) CALL PLOTIT (XSTATN,YNSTH,KMAX,0) *****
C ***** IF (INSTH.LT.0) CALL PLOTIT (XSTATN,YNSTH,NGKMAX,0) *****
C ***** WRITE (6,1003) TH(NTH) *****
C ***** IF (ICS.EQ.0) GO TO 7 *****
C ***** WRITE (6,1000) *****
C ***** IF (ICS.GT.0) CALL PLOTIT (XSTATN,YQS,KMAX,C) *****
C ***** IF (ICS.LT.0) CALL PLOTIT (XSTATN,YQS,NGKMAX,0) *****
C ***** WRITE (6,1004) TH(NTH) *****
C ***** IF (IMS.EQ.0) GO TO 8 *****
C ***** IF (IMS.GT.0) CALL PLOTIT (XSTATN,YMS,KMAX,C) *****
C ***** IF (IMS.LT.0) CALL PLOTIT (XSTATN,YMS,NGKMAX,0) *****
C ***** WRITE (6,1005) TH(NTH) *****
C ***** IF (IMTF.EQ.0) GO TO 9 *****
C ***** IF (IMTF.GT.0) CALL PLOTIT (XSTATN,YMTH,KMAX,0) *****
C ***** IF (IMTF.LT.0) CALL PLOTIT (XSTATN,YMTH,NGKMAX,0) *****
C ***** SAT20010 *****
C ***** SAT20020 *****
C ***** SAT20030 *****
C ***** SAT20040 *****
C ***** SAT20050 *****
C ***** SAT20060 *****
C ***** SAT20070 *****
C ***** SAT20080 *****
C ***** SAT20090 *****
C ***** SAT20100 *****
C ***** SAT20110 *****
C ***** SAT20120 *****
C ***** SAT20130 *****
C ***** SAT20140 *****
C ***** SAT20150 *****
C ***** SAT20160 *****
C ***** SAT20170 *****
C ***** SAT20180 *****
C ***** SAT20190 *****
C ***** SAT20200 *****
C ***** SAT20210 *****
C ***** SAT20220 *****
C ***** SAT20230 *****
C ***** SAT20240 *****
C ***** SAT20250 *****
C ***** SAT20260 *****
C ***** SAT20270 *****
C ***** SAT20280 *****
C ***** SAT20290 *****
C ***** SAT20300 *****
C ***** SAT20310 *****
C ***** SAT20320 *****
C ***** SAT20330 *****
C ***** SAT20340 *****
C ***** SAT20350 *****
C ***** SAT20360 *****
C ***** SAT20370 *****
C ***** SAT20380 *****
C ***** SAT20390 *****
C ***** SAT20400 *****
C ***** SAT20410 *****
C ***** SAT20420 *****
C ***** SAT20430 *****
C ***** SAT20440 *****
C ***** SAT20450 *****
C ***** SAT20460 *****
C ***** SAT20470 *****
C ***** SAT20480 *****

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      9      WRITE (6,1006) TH(NTH)
      IF (IMSTH.EQ.0) GO TO 1211
      WRITE (6,1000)
      IF (IMSTH.GT.0) CALL PLOTIT (XSTATN,YMSTH,KMAX,0)
      IF (IMSTH.LT.0) CALL PLOTIT (XSTATN,YMSTH,NGKMAX,0)
      WRITE (6,1007) TH(NTH)
      IF (IU.EQ.0) GO TO 10
      IF (IU.EQ.0) GO TO 10
      WRITE (6,1000)
      IF (IU.GT.0) CALL PLOTIT (XSTATN,YU,KMAX,0)
      IF (IU.LT.0) CALL PLOTIT (XSTATN,YU,NGKMAX,C)
      WRITE (6,1010) TH(NTH)
      IF (IV.EQ.0) GO TO 11
      IF (IV.EQ.0) GO TO 11
      WRITE (6,1000)
      IF (IV.GT.0) CALL PLOTIT (XSTATN,YV,KMAX,C)
      IF (IV.LT.0) CALL PLOTIT (XSTATN,YV,NGKMAX,C)
      WRITE (6,1009) TH(NTH)
      IF (IW.EQ.0) GO TO 12
      IF (IW.EQ.0) GO TO 12
      WRITE (6,1000)
      IF (IW.GT.0) CALL PLOTIT (XSTATN,YW,KMAX,0)
      IF (IW.LT.0) CALL PLOTIT (XSTATN,YW,NGKMAX,0)
      WRITE (6,1008) TH(NTH)
      IF (IPHIS.EQ.0) GO TO 13
      IF (IPHIS.EQ.0) GO TO 13
      WRITE (6,1000)
      IF (IPHIS.GT.0) CALL PLOTIT (XSTATN,YPHIS,KMAX,0)
      IF (IPHIS.LT.0) CALL PLOTIT (XSTATN,YPHIS,NGKMAX,0)
      WRITE (6,1011) TH(NTH)
      IF (IPHIT.EQ.0) GO TO 14
      IF (IPHIT.EQ.0) GO TO 14
      WRITE (6,1000)
      IF (IPHIT.GT.0) CALL PLOTIT (XSTATN,YPHIT,KMAX,0)
      IF (IPHIT.LT.0) CALL PLOTIT (XSTATN,YPHIT,NGKMAX,0)
      WRITE (6,1012) TH(NTH)
      IF (IPHI.EQ.0) GO TO 21
      IF (IPHI.EQ.0) GO TO 21
      WRITE (6,1000)
      IF (IPHI.GT.0) CALL PLOTIT (XSTATN,YPHI,KMAX,0)
      IF (IPHI.LT.0) CALL PLOTIT (XSTATN,YPHI,NGKMAX,0)
      WRITE (6,1013) TH(NTH)
      RETURN
      IF (INS.EQ.0) GO TO 15
      IF (INS.EQ.0) GO TO 15
      WRITE (6,1000)
      IF (INS.GT.0) CALL PLOTIT (XSTATN,YNS,KMAX,C)
      IF (INS.LT.0) CALL PLOTIT (XSTATN,YNS,NGKMAX,0)
      WRITE (6,2001)
      IF (INTF.EQ.0) GO TO 16
      IF (INTF.EQ.0) GO TO 16
      WRITE (6,1000)
      IF (INTF.GT.0) CALL PLOTIT (XSTATN,YNTH,KMAX,C)
      IF (INTF.LT.0) CALL PLOTIT (XSTATN,YNTH,NGKMAX,0)
      WRITE (6,2002)
      IF (INSTH.EQ.0) GO TO 17
      IF (INSTH.EQ.0) GO TO 17

```

SAT20490
 SAT20500
 SAT20510
 SAT20520
 SAT20530
 SAT20540
 SAT20550
 SAT20560
 SAT20570
 SAT20580
 SAT20590
 SAT20600
 SAT20610
 SAT20620
 SAT20630
 SAT20640
 SAT20650
 SAT20660
 SAT20670
 SAT20680
 SAT20690
 SAT20700
 SAT20710
 SAT20720
 SAT20730
 SAT20740
 SAT20750
 SAT20760
 SAT20770
 SAT20780
 SAT20790
 SAT20800
 SAT20810
 SAT20820
 SAT20830
 SAT20840
 SAT20850
 SAT20860
 SAT20870
 SAT20880
 SAT20890
 SAT20900
 SAT20910
 SAT20920
 SAT20930
 SAT20940
 SAT20950
 SAT20960


```

WRITE (6,1000)
IF (INSTH.GT.0) CALL PLOTIT (XSTATN,YNSTH,KMAX,0)
IF (INSTH.LT.0) CALL PLOTIT (XSTATN,YNSTH,NGKMAX,0)
17 IF (ICS.EQ.0) GO TO 18
WRITE (6,1000)
IF (IQS.GT.0) CALL PLOTIT (XSTATN,YQS,KMAX,C)
IF (IQS.LT.0) CALL PLOTIT (XSTATN,YQS,NGKMAX,C)
18 IF (IMS.EQ.0) GO TO 19
WRITE (6,1000)
IF (IMS.GT.0) CALL PLOTIT (XSTATN,YMS,KMAX,C)
IF (IMS.LT.0) CALL PLOTIT (XSTATN,YMS,NGKMAX,C)
19 IF (IMTH.EQ.0) GO TO 22
WRITE (6,2005)
IF (IMTH.GT.0) CALL PLOTIT (XSTATN,YMTH,KMAX,C)
IF (IMTH.LT.0) CALL PLOTIT (XSTATN,YMTH,NGKMAX,C)
22 IF (IMSTH.EQ.0) GO TO 231
WRITE (6,1000)
IF (IMSTH.GT.0) CALL PLOTIT (XSTATN,YMSTH,KMAX,0)
IF (IMSTH.LT.0) CALL PLOTIT (XSTATN,YMSTH,NGKMAX,0)
231 IF (IU.EQ.0) GO TO 23
WRITE (6,1000)
IF (IU.GT.0) CALL PLOTIT (XSTATN,YU,KMAX,C)
IF (IU.LT.0) CALL PLOTIT (XSTATN,YU,NGKMAX,C)
23 IF (IV.EQ.0) GO TO 24
WRITE (6,1000)
IF (IV.GT.0) CALL PLOTIT (XSTATN,YV,KMAX,C)
IF (IV.LT.0) CALL PLOTIT (XSTATN,YV,NGKMAX,C)
24 IF (IW.EQ.0) GO TO 25
WRITE (6,1000)
IF (IW.GT.0) CALL PLOTIT (XSTATN,YW,KMAX,C)
IF (IW.LT.0) CALL PLOTIT (XSTATN,YW,NGKMAX,C)
25 IF (IPHS.EQ.0) GO TO 26
WRITE (6,1000)
IF (IPHS.GT.0) CALL PLOTIT (XSTATN,YPHIS,KMAX,0)
IF (IPHS.LT.0) CALL PLOTIT (XSTATN,YPHIS,NGKMAX,0)
26 IF (IPHIT.EQ.0) GO TO 27
WRITE (6,1000)
IF (IPHIT.GT.0) CALL PLOTIT (XSTATN,YPHIT,KMAX,0)
IF (IPHIT.LT.0) CALL PLOTIT (XSTATN,YPHIT,NGKMAX,0)

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SAT2057C
 SAT20980
 SAT20990
 SAT21000
 SAT21010
 SAT21020
 SAT21030
 SAT21040
 SAT21050
 SAT21060
 SAT21070
 SAT21080
 SAT21090
 SAT21100
 SAT21110
 SAT21120
 SAT21130
 SAT21140
 SAT21150
 SAT21160
 SAT21170
 SAT21180
 SAT21190
 SAT21200
 SAT21210
 SAT21220
 SAT21230
 SAT21240
 SAT21250
 SAT21260
 SAT21270
 SAT21280
 SAT21290
 SAT21300
 SAT21310
 SAT21320
 SAT21330
 SAT21340
 SAT21350
 SAT21360
 SAT21370
 SAT21380
 SAT21390
 SAT21400
 SAT21410
 SAT21420
 SAT21430
 SAT21440


```

27 WRITE (6,2C12) GO TO 28
   IF (IPHI.EQ.0)
28 WRITE (6,1000)
   IF (IPHI.GT.0) CALL PLOTIT (XSTATN,YPHI ,KMAX,0)
   IF (IPHI.LT.0) CALL PLOTIT (XSTATN,YPHI ,NGKMAX,0)
   WRITE (6,2013)
   RETURN
C*****
1000 FCRMAT ('1',T10,'S'-'MEMBRANE FCRCE VS STATN, MERIDIAN AT THETA =',
1001 FCRMAT ('0',T10,'RADIANS',)
1002 FCRMAT ('0',T10,'S'-'MEMBRANE FCRCE VS STATN, MERIDIAN AT THETA =',
1003 FCRMAT ('0',T10,'RADIANS',)
1004 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
1005 FCRMAT ('0',T10,'RADIANS',)
1006 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
1007 FCRMAT ('0',T10,'RADIANS',)
1008 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
1009 FCRMAT ('0',T10,'RADIANS',)
1010 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
1011 FCRMAT ('0',T10,'RADIANS',)
1012 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
1013 FCRMAT ('0',T10,'RADIANS',)
2001 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2002 FCRMAT ('0',T10,'RADIANS',)
2003 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2004 FCRMAT ('0',T10,'RADIANS',)
2005 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2006 FCRMAT ('0',T10,'RADIANS',)
2007 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2008 FCRMAT ('0',T10,'RADIANS',)
2009 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2010 FCRMAT ('0',T10,'RADIANS',)
2011 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',
2012 FCRMAT ('0',T10,'RADIANS',)
2013 FCRMAT ('0',T10,'S'-'MEMBRANE FORCE VS STATN, MERIDIAN AT THETA =',

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```

WRITE (6,1000)
CALL PLCTIT (XSTATN,YDSTIF,NGKMAX,0)
WRITE (6,1007)
IF (IBBSTF.EQ.0) GO TO 10
5  WRITE (6,1000)
CALL PLCTIT (XSTATN,YBBSTF,NGKMAX,0)
WRITE (6,1008)
1C IF (IDCSTF.EQ.0) GO TO 1
WRITE (6,1000)
CALL PLCTIT (XSTATN,YDCSTF,NGKMAX,0)
WRITE (6,1009)
1 IF (IPR.EQ.0) GO TO 11
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPR,NGKMAX,0)
WRITE (6,1010)
11 IF (IPS.EQ.0) GO TO 12
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPS,NGKMAX,0)
WRITE (6,1011)
12 IF (IPT.EQ.0) GO TO 13
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPT,NGKMAX,0)
WRITE (6,1012)
13 IF (ITT.EQ.0) GO TO 14
WRITE (6,1000)
CALL PLCTIT (XSTATN,YTT,NGKMAX,0)
WRITE (6,1013)
14 IF (IMT.EQ.0) GO TO 15
WRITE (6,1000)
CALL PLCTIT (XSTATN,YMT,NGKMAX,0)
WRITE (6,1014)
15 IF (IDT.EQ.0) GO TO 16
WRITE (6,1000)
CALL PLCTIT (XSTATN,YDTT,NGKMAX,0)
WRITE (6,1015)
16 IF (ICMT.EQ.0) GO TO 17
WRITE (6,1000)
CALL PLCTIT (XSTATN,YDMT,NGKMAX,0)
WRITE (6,1016)
17 RETURN
*****
1000 FCRMAT ('1')
1001 FCRMAT ('0',T10,'RADIUS VS STATICA')
1002 FCRMAT ('0',T10,'GAMMA VS STATICA')
1003 FCRMAT ('0',T10,'OMEGA-S VS STATICA')
1004 FCRMAT ('0',T10,'OMEGA-THETA VS STATION')
1005 FCRMAT ('0',T10,'DECMEGA-S VS STATION')

```

SAT222410
 SAT222420
 SAT222430
 SAT222440
 SAT222450
 SAT222460
 SAT222470
 SAT222480
 SAT222490
 SAT222500
 SAT222510
 SAT222520
 SAT222530
 SAT222540
 SAT222550
 SAT222560
 SAT222570
 SAT222580
 SAT222590
 SAT222600
 SAT222610
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 SAT222630
 SAT222640
 SAT222650
 SAT222660
 SAT222670
 SAT222680
 SAT222690
 SAT222700
 SAT222710
 SAT222720
 SAT222730
 SAT222740
 SAT222750
 SAT222760
 SAT222770
 SAT222780
 SAT222790
 SAT222800
 SAT222810
 SAT222820
 SAT222830
 SAT222840
 SAT222850
 SAT222860
 SAT222870
 SAT222880


```

WRITE (6,34)
WRITE (6,35)
WRITE (6,36)
WRITE (6,37)
WRITE (6,38)
WRITE (6,39)
WRITE (6,40)
111 FCFMAT ('.',T11,'
1 FCFMAT ('.',T11,'
2 FCFMAT ('.',T11,'
3 FCFMAT ('.',T11,'
4 FCFMAT ('.',T11,'
5 FCFMAT ('.',T11,'
6 FCFMAT ('.',T11,'
7 FCFMAT ('.',T11,'
8 FCFMAT ('.',T11,'
9 FCFMAT ('.',T11,'
10 FCFMAT ('.',T11,'
11 FCFMAT ('.',T11,'
12 FCFMAT ('.',T11,'
13 FCFMAT ('.',T11,'
14 FCFMAT ('.',T11,'
15 FCFMAT ('.',T11,'
16 FCFMAT ('.',T11,'
17 FCFMAT ('.',T11,'
18 FCFMAT ('.',T11,'
19 FCFMAT ('.',T11,'
20 FCFMAT ('.',T11,'
21 FCFMAT ('.',T11,'
22 FCFMAT ('.',T11,'
23 FCFMAT ('.',T11,'
24 FCFMAT ('.',T11,'
25 FCFMAT ('.',T11,'
26 FCFMAT ('.',T11,'
27 FCFMAT ('.',T11,'
28 FCFMAT ('.',T11,'
29 FCFMAT ('.',T11,'
30 FCFMAT ('.',T11,'
31 FCFMAT ('.',T11,'
32 FCFMAT ('.',T11,'
33 FCFMAT ('.',T11,'
34 FCFMAT ('.',T11,'
35 FCFMAT ('.',T11,'
36 FCFMAT ('.',T11,'
37 FCFMAT ('.',T11,'
38 FCFMAT ('.',T11,'
39 FCFMAT ('.',T11,'
40 FCFMAT ('.',T11,'
41 FCFMAT ('.',T11,'
42 FCFMAT ('.',T11,'
43 FCFMAT ('.',T11,'
44 FCFMAT ('.',T11,'
45 FCFMAT ('.',T11,'
46 FCFMAT ('.',T11,'
47 FCFMAT ('.',T11,'
48 FCFMAT ('.',T11,'
49 FCFMAT ('.',T11,'
50 FCFMAT ('.',T11,'
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100 FCFMAT ('.',T11,'

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AND PANDD(K,MN) TO SET UP THE P, P-BAR AND P-HAT MATRICES GIVEN
BY EQUATIONS (30).
INTERNALLY, MATRICES DL, DG AND DF ARE SET UP FOR THE CALCULA-
TION OF X(I) GIVEN BY EQUATION (31A), WHERE
X(I) = DL*SMALL-L(I) + DG*SMALL-G(I) + DF*SMALL-F(I)
THE SPECIAL P MATRIX FOR A SHELL WITH AN INITIAL FCLE IS ALSO
COMPUTED HERE.
MATRICES ZF1M, ZF2M, ZF3M, ZF4M ARE SET UP FOR THE CALCULATION OF
Z(K+1) GIVEN BY EQUATION (31B), WHERE
Z(K+1)=ZF1M*SMALL-L(K) + ZF2M*X(K) + ZF3M*X(K-1) + ZF4M*SMALL-
IF THE SHELL HAS A FINAL POLE, THE MATRICES CLC,CL1,CL2 ARE
PREPARED FOR THE CALCULATION CF Z(K)
*****
REAL JAY
DIMENSION P(4,4,1),DEE(4,4,1),DST(4,4,1),X(4,1),ZC(4,1),
1 Z2(4,1),Z3(4,1)
CCMCON /IBL1/ MNMAX
CCMCON /IBL2/ N(99),MNINIT
CCMCON /IBL3/ MO,M1,M2,M3
CCMCON /IBL4/ KMAX,KL
CCMCON /IBL5/ IBCINL,IBCFNL
CCMCON /IBL1/ A(4,4),BEE(4,4),C(4,4,99),
CCMCON /IBL4/ ZF1M(4,4,99),ZF2M(4,4,99),
1 ZF3M(4,4,99),ZF4M(4,4,99)
CCMCON /BL13/ OMEGL(4,4),CAPL1(4,4),OMEGL(4,4),CAPLL(4,4),
1
CCMCON /BL23/ JAY(4,4),F(4,4,99),DF(4,4,99)
CCMCON /BL24/ DL(4,4,99),DG(4,4,99)
CCMCON /BL25/ E(4,4),F(4,4),P(4,4),G(4,4)
1 DIMENSION PATA(4,4,4),PBTA(4,4,4),PQTA(4,4,4),PIR(4,
2 T(4),CGG(4,4),ZF1(4,4,4),ZF2(4,4,4),ZFPC(4,4,4),ZFP1(4,4),IFIVC
ECLIVALENCE (CLO(1),ZFLM(1)),CL1(4,4),CL2(4,4),G1(4,
1 (ZFPO(1),PATA(1)),(ZFPL(1),PBTA(1)),(CL2(1),ZF3M(1)),
2 (ZF1(1),DLL(1)),(ZF2(1),PIR(1))
*****
IF (IBCFNL.LT.0) GO TO 10
CC 1 AN=MNINIT,MNMAX
CALL FJG(1,MN)
CALL EFG(1,MN,ZO,Z2,Z3)
CALL ABC
1=1,4
3 J=1,4
CC

```



```

4      SUMA=0.
      SUMB=0.
      SUMC=0.
      L=1,4
      SUMJ=SUMA+C(I,L)*JAY(L,J)
      SUMB=SUMB+C(I,L)*BEE(L,J)
      SUMC=SUMC+CMEGL(I,L)*H(L,J)
      PATA(I,J)=SUMA+UNIT(I,J)
      PETA(I,J)=SUMB
      PCTA(I,J)=SUMC
      PCTA(I,J)=SUMJ
      I=1,4
      J=1,4
      SUMCB=0.
      SUMCA=0.
      SUMCC=0.
      L=1,4
      SUMCB=SUMCB+POTA(I,L)*PBTA(L,J)
      SUMCA=SUMCA+POTA(I,L)*PATA(L,J)
      SUMCC=SUMCC+POTA(I,L)*C(L,J)
      CL(I,J)=SUMCB+PCTA(I,J)+CAPL1(I,J)
      PTR(I,J)=SUMOA
      LGG(I,J)=SUMOC
      CALL MATINV(DLL,4,PTR,4,DETERM,IPIVOT,INDEX,4,ISCALE)
      I=1,4
      J=1,4
      SUMD=0.
      SUME=0.
      L=1,4
      SUMD=SUMD+DLL(I,L)*DGG(L,J)
      SUME=SUME-DLL(I,L)*CMEGL(L,J)
      CL(I,J,MN)=DLL(I,J)
      CG(I,J,MN)=SUMD
      DF(I,J,MN)=SUME
      I=1+K*MAX*(MN-1)
      J=1,4
      P(I,J,I,J)=PTR(I,J)
      CG(I,J,I,J)=1,4
      L=1,4
      MN=MNINIT,MNMAX
      NN=IABS(N(MN))
      IJ=1+K*MAX*(MN-1)
      CC(I,J,I,J)=1,4
      X(I,I,J)=0.
      L=1,4
      J=1,4
      P(I,J,I,J)=0.
      IF(NN.GT.3) GO TO 11
      IF(NN.GT.2) GO TO 50

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00002100
00002110
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00002130
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00002200
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00002240
00002250
00002260
00002270

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C      IN  FMATRX
CALL EFG(2,MN,ZG,Z2,Z3)
CALL ABC
CALL MATINV(A,4,G1,0,DETERM,IPIVCT,INDEX,4,ISCALE)
CC 501 II=1,4
DC 501 JJ=1,4
CL(1,1,1,MN)=0.
EG(1,1,1,MN)=0.
CF(1,1,1,MN)=0.
IF(IN.GT.1) GO TO 12
IF(IN.GT.0) GO TO 13
MC=MN
CL(1,1,MN)=1.
CL(1,2,MN)=1.
CL(2,3,MN)=-3.
CL(3,4,MN)=-3.
CG(3,3,MN)=4.
CG(4,4,MN)=4.
CF(3,3,MN)=-1.
CF(4,4,MN)=-1.
CC TO SC2
13 M1=MN
CL(1,1,MN)=-3.
CL(2,1,MN)=1.
CL(2,2,MN)=1.
IF(N(M1).LT.0)DL(2,2,MN)=-1.
CL(3,3,MN)=1.
CL(4,4,MN)=1.
CG(1,1,MN)=4.
CF(1,1,MN)=-1.
CC TO SC2
12 M2=MN
CL(1,1,MN)=1.
CL(2,2,MN)=1.
CL(3,3,MN)=1.
CL(4,4,MN)=-3.
CG(4,4,MN)=4.
CF(4,4,MN)=-1.
CC INUE
DC 503 II=1,4
DC 503 JJ=1,4
TTF=0.
CC 504 L=1,4
TTF=1TP+DF(1,1,MN)*A(L,JJ)
CC 505 II=1,4
CC 505 JJ=1,4
TTF=0.
SC4
SC3

```



```

ITC=0.
CC SC6 L=1,4
ITF=ITP+CLO(II,L)*C(L,JJ)
ITQ=ITQ+CLO(II,L)*BEE(L,JJ)
CL1(II,JJ)=DL(II,JJ,MN)-ITP
CL2(II,JJ)=DG(II,JJ,MN)-ITQ
CALL MATINV(CLL,4,GI,0,DETERM,IPIVOT,INDEX,4,ISCALE)
CC SC7 II=1,4
CC SC7 JJ=1,4
ITP=0.
ITQ=0.
ITC=C.
CC SC8 L=1,4
ITF=ITP+CCL(II,L)*CLO(L,JJ)
ITQ=ITQ+CCL(II,L)*CL2(L,JJ)
CL(II,JJ,MN)=-ITP
P(II,JJ,IJ)=ITQ
GC TO 11
SC N2=MN
CCNTI=NUE
KLAST=KMAX
IF(IBCFL.LT.0) KLAST=KL
CC 23 K=2,KLAST
CC 23 MN=MNINIT,MNMAX
CALL EFG(K,MN,ZC,Z2,Z3)
CALL ABC
CALL FANDD(K,MN,P,CEE,DST,X)
IF(IBCFL.LT.0) GC TO 30
CC 40 MN=MNINIT,MNMAX
IKL=MN*KMAX-1
JKL=KMAX*MN
CALL FJ(KMAX,MN)
CC 41 I=1,4
CC 41 J=1,4
SUNC=0.
SUMP=0.
SUNJ=0.
CC 42 L=1,4
SUNC=SUMP+P(I,L,IKL)*H(L,J)
SUMP=SUMP+P(I,L,IKL)*F(L,J,JKL)
SUNJ=SUNJ+CMGL(I,L)*JAY(L,J)
PATA(I,J)=SUMO
PETA(I,J)=UNIT(I,J)-SUMP
CC 43 I=1,4
CC 43 J=1,4
SUMP=0.
SUNJP=0.
SUNCM=0.

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00002430
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00002500
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00003210
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CCMCMCN /IBL5/ IBCINL, IBCFNL
CCMCMCN /IBL8/ LSTEP, ITR
CCMCMCN /IBL12/ KMAX1, KMAX2, NCONV
CCMCMCN /IBL13/ ITRMAX, LSMAX
CCMCMCN /BL3/ PR(99), PX(99), PT(99)
CCMCMCN /BL4/ ZF1M(4,4,99), ZF2M(4,4,99),
1 ZF3M(4,4,99), ZF4M(4,4,99)
CCMCMCN /BL5/ TT(99), MT(99), DT(99), CMT(99)
CCMCMCN /BL6/ SQE, GSE, ALOAD
CCMCMCN /BL7/ DL, SL
CCMCMCN /BL8/ R(500), GAM(500), CMT(500)
CCMCMCN /BL9/ FFS(4,99), ELIS(4), GEES(4,99)
CCMCMCN /BL11/ OMXI(500), PHEE, TO, T2
CCMCMCN /BL12/ TDLI, TDEL
CCMCMCN /BL14/ LAM2, LSD18, LSDIN
CCMCMCN /BL15/ NU, UI(99), VI(99), W1(99), V2(99), W2(99), U2(99), U3(99),
1 V3(99), W3(99)
CCMCMCN /BL17/ DEL
CCMCMCN /BL24/ DL(4,4,99), DG(4,4,99), DF(4,4,99)
CCMCMCN /BL27/ BX3(99), BT3(99), BXT3(99), BE3(99)
CCMCMCN /BL28/ EXX3(99), ET13(99), ETX3(99), EX13(99), ET3(99)
CCMCMCN /BL29/ BX1(99), BT1(99), BXT1(99), BE1(99), BX2(99), BT2(99),
1 BX12(99), BE2(99)
CCMCMCN /BL30/ EXX1(99), ET11(99), ETX1(99), EX1(99), ET1(99), EXX2(99),
1 ET12(99), ETX2(99), EX2(99), ET2(99)
CCMCMCN /BL31/ DELSC, EXT1(99)
CCMCMCN /BL100/ TEEQ, $DYNMC
CCMCMCN /BL101/ DELSD
CCMCMCN /BL102/ DELLOAD
CCMCMCN /BL103/ MASS(500)
DIMEASICN GEE(4)
C*****FCIFF(A,B,C)=(-1.5*A+2.*B-.5*C)/DEL
RS=R(K)
RF=1./RS
GA=GAM(K)
CX=CMXI(K)
CT=CMT(K)
C12=D1*LAM2
CALL BCB(K,BS,DBS,D,DD)
CALL PLCAD(K,Z)
CALL TLCCAD(K,Z)
MAS=MASS(K)
CC 4 A=1, MNMAX
I2=K+1+(M-1)*KMAX2
IK=K+(M-1)*KMAX
IK1=IK-1
EN=A(M)
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00003720

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00003780

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00003980
00003990
00004000
00004010
00004020
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00004080
00004090
00004100
00004110
00004120
00004130
00004140
00004150

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```

ENR=ENR*RR
ENT=MT(M)
GEE(1)=(-PX(M)+DT(M)-DL2*GA*QX*EMT)*TDEL*ALCAD/DELSO
1 GEE(2)=(-5.*ZO(1,IZ)+4.*Z2(1,IZ)-Z3(1,IZ))*TDEL*ALCAD/DELSO
1 GEE(3)=(-5.*ZO(2,IZ)+4.*Z2(2,IZ)-Z3(2,IZ))*TDEL*ALCAD/DELSO
1 GEE(4)=(-PR(M)-CX*GT)*TT(M)-CL2*(GA*DMT(M)-(CX*GT-ENR**2)
1 *MT(M)))*TDEL*ALCAD
1 GEE(5)=(-5.*ZO(3,IZ)+4.*Z2(3,IZ)-Z3(3,IZ))*TDEL*DELSO
1 IF(ITRMAX.EQ.1) GO TO 5C
IF(K.GT.1) GO TO 6
BX2T=BX1(M)
BT2T=BT1(M)
BE2T=BE1(M)
ET2T=ET1(M)
EX2T=EX1(M)
ETX2T=ETX1(M)
BX3T=BX2(M),BX3(M)
BT3T=BT2(M),BT3(M)
BE3T=BE2(M),BE3(M)
ET3T=ET2(M),ET3(M)
EX3T=EX2(M),EX3(M)
ETX3T=ETX2(M),ETX3(M)
GO TO 7
6 IF(K.LT.KMAX) GO TO 8
BX2T=BX3(M)
BT2T=BT3(M)
BE2T=BE3(M)
ET2T=ET3(M)
EX2T=EX3(M)
ETX2T=ETX3(M)
BX1T=BX2T, BX1(M)
BT1T=BT2T, BT1(M)
BE1T=BE2T, BE1(M)
ET1T=ET2T, ET1(M)
EX1T=EX2T, EX1(M)
ETX1T=ETX2T, ETX1(M)

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00004630

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C**          9C3  L=1,4
C**          9C2  SUMX=SUMX+CL(I,I,L,M)*GEE(L,I)
C**          9C1  X(I,I,IK1)=SUMX
C**          C**  CCNTINUE
C**          C**  CC  I1 I=1,4
C**          C**  SUMX=0.
C**          C**  CC  I2 J=1,4
C**          C**  SUMX=SUMX+DEE(I,J,IK)*GEE(J,I,J,IK)*X(J,IK1)
C**          C**  X(I,I,IK)=SUMX
C**          C**  CC  I1 I=1,4
C**          C**  RETURN
C**          C**  ENCL
C**          C**  SUBROUTINE UPDATE
C**          C**  *****
C**          C**  THIS SUBROUTINE UPDATES THE STORAGE LCCATIONS OF THE BETA'S ANCD
C**          C**  ETAT. S. IT IS CALLED IN SUBROUTINE XANCLZ AFTER A MERICIAN
C**          C**  STATION CHANGE.
C**          C**  *****
C**          C**  CCMMCN /IBL1/ MNMAX
C**          C**  CCMMCN /BL27/ BX3(55),BT3(55),BX12(99),BE3(55)
C**          C**  CCMMCN /BL28/ EXX3(99),ET13(99),ETX3(99),EX2(99),ET2(99)
C**          C**  CCMMCN /BL29/ BX1(55),BT1(99),BX11(99),BE1(59),BX2(99),BT2(99),
C**          C**  1 CCMMCN /BL30/ BX12(99),BE2(55)
C**          C**  1 CCMMCN /BL30/ EXX1(99),ET11(99),ETX1(99),EX1(59),EX2(99),ET2(99)
C**          C**  CCMMCN /BL31/ DELSQ,ET11(99)
C**          C**  *****
C**          C**  CC  I M=1,MNMAX
C**          C**  BX1(M)=BX2(M)
C**          C**  BX11(M)=BT2(M)
C**          C**  BX11(M)=BX12(M)
C**          C**  BE1(M)=BE2(M)
C**          C**  BX2(M)=BX3(M)
C**          C**  BT2(M)=BT3(M)
C**          C**  BX12(M)=BX13(M)
C**          C**  BE2(M)=BE3(M)
C**          C**  EXX1(M)=EXX2(M)
C**          C**  ET11(M)=ET12(M)
C**          C**  ETX11(M)=ETX2(M)
C**          C**  EXX1(M)=EX2(M)
C**          C**  ET11(M)=ET2(M)
C**          C**  EXX2(M)=EXX3(M)
C**          C**  ET12(M)=ET13(M)
C**          C**  ETX2(M)=ETX3(M)
C**          C**  EXX2(M)=EX3(M)
C**          C**  ET2(M)=ET3(M)
C**          C**  1 ET2(M)=ET3(M)

```



```

6C 100 K=1,N
7C IF (IPIVOT(K)-1) 80, 100, 740
8C IF (ABS(AMAX)-ABS(A(J,K))) 85, 10C, 100
9C IFCW=J

```

```

10C ICCLUM=K
11C AMAX=A(J,K)
12C CCNTINUE
13C CCNTINUE
14C IF IPIVOT(ICCLUM)=IPIVCT(ICCLUM)+1

```

INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGNAL

```

130 IF (IROW-ICCLUM) 140, 260, 140
140 CTERM=-CTERM
150 CC 200 L=1,N
16C SWAP=A(IROW,L)
17C A(IROW,L)=A(ICCLUM,L)
20C A(ICCLUM,L)=SWAP
21C IF(M) 260, 260, 210
22C CC 250 L=1, M
23C SWAP=B(IROW,L)
24C B(IROW,L)=B(ICCLUM,L)
25C B(ICCLUM,L)=SWAP
26C INDEX(I,1)=IROW
27C INDEX(I,2)=ICCLUM
31C PIVCT=A(ICCLUM,ICCLUM)

```

SCALE THE DETERMINANT

```

10CC PIVCTI=PIVOT
10C5 IF (ABS(CTERM)-R1) 1030, 1010, 1010
101C CTERM=CTERM/R1
102C ISCALE=ISCALE+1
102C IF (ABS(CTERM)-R1) 1060, 1020, 102C
102C CTERM=CTERM/R1
102C ISCALE=ISCALE+1
103C GC TO 1060
104C IF (ABS(CTERM)-R2) 1040, 1040, 1060
104C CTERM=CTERM*R1
105C ISCALE=ISCALE-1
105C IF (ABS(CTERM)-R2) 1050, 1050, 1060
105C CTERM=CTERM*R1
105C ISCALE=ISCALE-1
106C IF (ABS(PIVCTI)-R1) 1090, 1070, 1070
107C PIVCTI=PIVCTI/R1
107C ISCALE=ISCALE+1
108C IF (ABS(PIVCTI)-R1) 320, 1080, 1080
108C PIVCTI=PIVCTI/R1

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00006000
00006010
00006020
00006030
00006040
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00006080
00006090
00006100
00006110
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00006360
00006370
00006380
00006390
00006400
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00006420
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00006440
00006450
00006460
00006470

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```

105C ISCALE=ISCALE+1
200C GC TO 320
IF (ABS(PIVOTI)-R2)200C,2000,320
PIVCTI=PIVCTI#R1
ISCALE=ISCALE-1
201C IF (ABS(PIVOTI)-R2)2010,201C,320
PIVCTI=PIVCTI#R1
ISCALE=ISCALE-1
320 CETERM=DETERM*PIVOTI

C C C
C DIVIDE PIVCT ROW BY PIVCT ELEMENT
C
330 A(ICOLU,ICCLUM)=1.0
340 DC 350 L=1,N
350 A(ICCLUM,L)=A(ICOLU,L)/PIVCT
360 IF (M) 380, 380, 360
370 DC 370 L=1,M
37C E(ICOLU,L)=B(ICOLU,L)/PIVCT

C C C
C REDUCE NON-PIVOT RCWS
C
38C DC 550 LI=1,N
39C IF (LI-ICOLU) 400, 550, 400
40C T=A(LI,ICOLU)
41C A(LI,ICCLUM)=0.0
42C DC 450 L=1,N
430 A(LI,L)=A(LI,L)-A(ICCLUM,L)*T
44C IF (M) 550, 550, 460
45C DC 500 L=1,M
46C B(LI,L)=B(LI,L)-B(ICCLUM,L)*T
47C CCNTINUE

C C C
C INTERCHANGE COLUMNS
C
60C DC 710 I=1,N
61C L=N+1-I
62C IF (INDEX(L,1)-INDEX(L,2)) 630, 710, 630
63C JFCW=INDEX(L,1)
64C JCCLUM=INDEX(L,2)
65C CC 705 K=1,N
66C SWAP=A(K,JROW)
67C A(K,JROW)=A(K,JCOLUM)
700C A(K,JCOLUM)=SWAP
71C CCNTINUE
72C CCNTINUE
73C RETURN
74C ENC
SUBROUTINE INLPCL (Z,PT-IXB,PHITB)

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BX1(M2)=BET
BT1(M2)=-BET
EXT1(M2)=-BET
ETX1(M1)=Q1
IF(M3.EQ.0) GO TO 2
EXX1(M3)=Q1
ETX1(M3)=-Q1
2 TC=0.
IF(M0.EQ.0) GO TO 3
BX1(M0)=BET
BT1(M0)=BET
CALL BCE(1,B,DB,D,CC)
CALL TLCCAD(1,Z)
I2=2+(M0-1)*KMAX2
I3=I2+1
I4=I3+1
TC=B*SI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+CMXI(1)*Z(3,I2)
1+.5*SOE*BET)-TT(M0)*ALCCAD
3 EXX1(M1)=PTEE*(T0+.5*T2)
RETURN
10CC CCNTINUE
PTEE=(1.5*Z(3,I2)-2.*Z(3,I3)+.5*Z(3,I4))/DEL+CMXI(1)*Z(1,I2)
T2=C.
IF(M2.EQ.0) GO TO 1002
CALL BDE(1,B,DB,D,CC)
I2=2+(M2-1)*KMAX2
I3=I2+1
I4=I3+1
PTX1=PHIXB(KMAX+1)
PTX2=PHIXB(2*KMAX+1)
PFEN=(1.5*Z(3,I2-KMAX2)-2.*Z(3,I3-KMAX2)+.5*Z(3,I4-KMAX2))/DEL+
1CMXI(1)*Z(1,I2-KMAX2)
BX1(M2)=.5*(PTEE*(PTX1)-PFEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.0.1) BX1(M2)=0.
BT1(M2)=-BX1(M2)
EXT1(M2)=-BX1(M2)
T2=B*DI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+.5*SOE*BX1(M2))
M2L=M2-1
EXX1(M2L)=PTEE*(PTEN+PHX2)+PHX1*PTEN
IF(ITRMAX.EQ.0.1) BX1(M2L)=0.
BT1(M2L)=-BX1(M2L)
EXT1(M2L)=BX1(M2L)
T2A=B*CI*((-1.5*Z(1,I2-KMAX2)+2.*Z(1,I3-KMAX2)-.5*Z(1,I4-KMAX2))
1/DEL+.5*SOE*BX1(M2L))
1002 TC=C.
IF(M0.EQ.0) GO TO 1003
BX1(M0)=.5*(PTEE*(PTX1)+PTEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.0.1) BX1(M0)=0.

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00008380
00008390

BT1(M0)=BX1(M0)
CALL BCE(1,B,DB,D,DC)
CALL TLCD(1,Z)
I2=2+(MC-1)*KMAX2
I3=I2+1
I4=I3+1
ITC=B*SL1*B*SL1*(1,13)-.5*Z(1,I4))/DEL+CMXI(1)*Z(3,I2)
1+.5*SQRT(1,13)-.5*Z(1,I4))/DEL+CMXI(1)*Z(3,I2)
10C3 IF(ITRMAX.EQ.1) GC TC 1001
PFSS=PFEE+PHX1
PHSP=PHEN+PHX2
MIL=M1-1
EXXI(M1)=PHSS*T0+.5*(PHSS*T2+PHSP*T2N)
EXXI(M1)=PHSP*T0-.5*(PHSP*T2+PHSS*T2N)
ETXI(M1)=.5*(PHSS*T2+PHSP*T2N)
ETXI(M1)=.5*(-PHSP*T2+PHSS*T2N)
IF(M3.EQ.0) GO TO 1001
NXL=N3-1
EXXI(M3)=.5*(PHSS*T2+PHSP*T2N)
EXXI(M3)=.5*(PHSS*T2N+PHSP*T2)
ETXI(M3)=.5*(-PHSP*T2+PHSS*T2N)
ETXI(M3)=.5*(-PHSP*T2+PHSS*T2N)
CCCONTINUE
10C1 RETURN
END
SUBROUTINE ABC
***** THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE A, BEE, ANC C
***** MATRICES. *****
***** COMMON /BL1/ A(4,4),BEE(4,4),C(4,4) *****
***** COMMON /BL2/ TCEL,TDCEL *****
***** COMMON /BL17/ TCEL,TDCEL *****
***** COMMON /BL25/ E(4,4),F(4,4),G(4,4) *****
***** Z=2./DEL *****
CC 1 I=1,4
CC 1 J=1,4
CC CEIJ=D2*E(I,J)
F(I,J)=F(I,J)-2.*DEIJ+TCEL*G(I,J)
BEE(I,J)=DEIJ-F(I,J)
C(I,J)=CEIJ-F(I,J)
1 RETURN
END
SUBROUTINE PANDD(K,MN,P,DEE,DST,X)
***** THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE P, P-BAR, AND
*****
C
C
C

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C** P-HAT MATRICES FOR EACH MEDICIAN STATION K AND FOURIER MCCE MN*00008400
C** THESE MATRICES ARE COMPUTED AND SAVED BECAUSE THEY DC NCT *00008410
C** CHANGE DURING EITHER THE ITERATION PROCEDURE OR THE LOAD INCRE-00008420
C** WENT PROCEDURE - AS THEY ARE A FUNCTION OF THE SPELL'S INITIAL*00008430
C** GEOMETRY AND STIFFNESS. *00008440
C** DIMENSION P(4,4,1), DEE(4,4,1), DST(4,4,1), X(4,1) *00008450
C** CCMMCN /IBL4/ KMAX, KL *00008460
C** CCMMCN /BL1/ A(4,4,99), ZF2M(4,4,99), *00008470
C** CCMMCN /BL4/ ZF1M(4,4,99), ZF4M(4,4,99) *00008480
C** 1 DIMENSION TM(4,4), IPIVCT(4), INDEX(4,2), X2(4) *00008510
C** IKL=K+KMAX*(MN-1) *00008520
C** KLI=IKL-1 *00008530
C** DO 1 I=1,4 *00008540
C** DO 1 J=1,4 *00008550
C** SUM=0. *00008560
C** DO 2 L=1,4 *00008570
C** SUM=SUM+C(I,L)*P(L,J,KLI) *00008580
C** TM(I,J)=BEE(I,J)-SUM *00008590
C** 1 CALL MATINV(TM,4,X2,0,DETERM,IPIVCT,INDEX,4,ISCALE) *00008600
C** DO 3 I=1,4 *00008610
C** DO 3 J=1,4 *00008620
C** SUMA=0. *00008630
C** DO 4 L=1,4 *00008640
C** SUMA=SUMA+TM(I,L)*A(L,J) *00008650
C** SUMC=SUMC+TM(I,L)*C(L,J) *00008660
C** SUMC=SUMC+SUMA *00008670
C** 6 P(I,J,IKL)=SUMC *00008680
C** DEET(I,J,IKL)=TM(I,J) *00008690
C** DEET(I,J,IKL)=SUMC *00008700
C** 5 RETURN *00008710
C** ENCL *00008720
C** SUPERROUTINE FNLPOL (Z,PHIXB,PHITB) *00008730
C** *00008740
C** *00008750
C** THIS SUBROUTINE COMPUTES THE NCN-LINEAR TERMS BETA-SUB S, *00008760
C** -SUB THETA, -SUB S-THETA, ETA-SUB S-S, AND -SUB THETA-S AT A *00008770
C** FINAL PCLE. *00008780
C** *00008790
C** *00008800
C** DIMENSION Z(4,1), PHIXB(1), PHITB(1) *00008810
C** CCMMCN /IBL1/ MNMAX *00008820
C** CCMMCN /IBL3/ M0,M1,M2,M3 *00008830
C** CCMMCN /IBL4/ KMAX, KL *00008840
C** CCMMCN /IBL12/ KMAX1,KMAX2,NCONV *00008850
C** CCMMCN /IBL13/ ITRMAX,LSMAX *00008860
C** CCMMCN /IBLJ/ JUMP *00008870
C** TT(99),EMT(99),DT(99),DMT(99)

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TC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+CMXI(KMAX))*
12(3,KM)+.5*SDE*BE1)-TT(MO)*ALOAD
3 EXX3(M1)=PHEE*(TO+.5*TT)
RETURN
C*****
1000 CCNTINUE
12=C. EQ.0) GO TO 1002
IF(M2.EQ.0) GO TO 1002
KM=KMAX1+(M2-1)*KMAX2
KM1=KM-1
KM2=KM-2
J=KMAX*2
I=J+KMAX
PHX1=PHIXB(J)
PHX2=PHIXB(I)
PHEN=-((1.5*Z(3,KM-KMAX2)-2.*Z(3,KM1-KMAX2)+.5*Z(3,KM2-KMAX2))/DEL
1+CMXI(KMAX))*Z(1,KM-KMAX2)
BX3(M2)=.5*(PHEE*(PHEN+2.*PHX1)-PHEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX3(M2)=0.
ET3(M2)=-BX3(M2)
BX13(M2)=BX3(M2)
M2L=M2-1
BX3(M2L)=PHEE*(PHEN+PHX2)+PHX1*PHEN
IF(ITRMAX.EQ.1) BX3(M2L)=0.
ET3(M2L)=-BX3(M2L)
BX13(M2L)=-BX3(M2L)
12=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+.5*SCE*BX3(M2))
12N=B*CI*((1.5*Z(1,KM-KMAX2)-2.*Z(1,KM1-KMAX2)+.5*Z(1,KM2-KMAX2))
1/DEL+.5*SDE*BX3(M2L))
1002 TC=C.
IF(MO.EQ.0) GO TO 1003
CALL TLCD(KMAX,Z)
KM=KMAX1+(MO-1)*KMAX2
KM1=KM-1
KM2=KM-2
BX3(MO)=.5*(PHEE*(PHEN+2.*PHX1)+PHEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX3(MO)=0.
ET3(MO)=BX3(MO)
TC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+CMXI(KMAX))*
1 Z(3,KM)+.5*SDE*BE1)-TT(MO)*ALOAD
1003 IF(ITRMAX.EQ.1) GO TO 1001
PHSS=PHEN+PHX1
PHSP=PHEN+PHX2
M1L=M1-1
EXX3(M1)=PHSS*TO+.5*(PHSS*TT2+PHSP*TT2N)
EXX3(M1L)=PHSP*TO-.5*(PHSP*TT2-PHSS*TT2N)
ETX3(M1)=.5*(PHSS*TT2+PHSP*TT2N)
ETX3(M1L)=.5*(-PHSP*TT2+PHSS*TT2N)

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IF(M3.EQ.0) GO TO 1001
M3L=M3-1
EXX3=(M3)=.5*(PHSS*T2-PHSP*T2N)
ETX3=(M3L)=.5*(PHSS*T2N+PHSP*T2)
ETX3=(M3)=.5*(-PHSS*T2+PHSP*T2N)
ETX3=(M3L)=.5*(-PHSP*T2-PHSS*T2N)
1001 CCNTINUE
RETURN
END
SUBROUTINE PHIBET(K,Z,IS,JS,ID,JD,PHIXB,PHITB)
*****
C THIS SUBROUTINE CALCULATES THE PHI'S AND CARRIES CLT THE BETA
C MULTIPLYING AND SUMMATION PROCEDURE FOR COMPUTING THE BETA
C NCN-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
C IS, ID, JS, IJS, MAXS, MAXC, MAXSY ARE PREPARED IN SUB-
C ROUTINE NCDES AND USED HERE.
*****
C DIMENSION Z(4,1), IS(99,1), JS(99,1), ID(99,1), JD(99,1), PHIXB(1),
C PHITB(1)
1 PHITB(1)
C COMMON /IBL1/ MNMAX
C COMMON /IBL2/ N(99), MNINIT
C COMMON /IBL4/ KMAX, KL
C COMMON /IBL7/ MNMAXO, MAXD(99), MAXS(59), MAXSY(59), IJS(59)
C COMMON /IBL12/ KMAX1, KMAX2, NCONV
C COMMON /IBL13/ ITRMAX, LSMAX
C COMMON /IBLJ/ JUMP
C COMMON /IBL6/ SOE, CSE, ALCAD
C COMMON /BL8/ R(500), GAM(500), OMT(500)
C COMMON /BL10/ PHIX(99), PHIT(99), PHI(99)
C COMMON /BL11/ OMXI(500), PHEE, TO, T2
C COMMON /BL12/ TDLI, TDEL
C COMMON /BL15/ NU, UI(99), V1(99), V2(59), U2(59), W2(59), U3(59),
C V3(99), W3(99)
C COMMON /BL27/ BX3(59), BT3(99), BXT3(99), BE3(59)
C COMMON /BLPHS/ PHX(99), PHT(99)
*****
C X=CMXI(K)
C T=CMT(K)
RPA=1./R(K)
GA=GAM(K)
KF2=K+2
CC 1 M=1, MNMAXO
EN=N(M)
IK=KP2+(M-1)*KMAX2
U3(M)=Z(1,IK)
V3(M)=Z(2,IK)
W3(M)=Z(3,IK)
PHIX(M)=-TDLI*(W3(M)-W1(M))+CX*L2(M)
*****

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1 PHIT(M)=EN*W2(M)*RRRA+V2(M)*CT
  PHI(M)=(TDLI*(V3(M)-V1(M))+GA*V2(M)+EN*U2(M)*RRRA)*.5
  IF(ITRMAX.EQ.1) RETURN
  IF(JUMP.EQ.2) GO TO 1111
  CC 5 N=1,MNMAX
  SMC=0.
  SMT=0.
  SMF=0.
  IF(N(M).EQ.0) GO TO 20
  MAXL=MAXS(M)
  IF(MAXL.EQ.0) GO TO 2
  CC 3 L=1,MAXL
  I=IS(L,M)
  J=JS(L,M)
  SMC=SMO+PHIX(I)*PHIX(J)
  SMT=SMT+PHIT(I)*PHIT(J)
  SMF=SMR+PHIX(I)*PHIT(J)+PHIX(J)*PHIT(I)
  SMC=SMF-PHI(I)*PHI(J)
  MAXL=MAXC(M)
  IF(MAXL.EQ.0) GO TO 4
  CC 5 L=1,MAXL
  I=IC(L,M)
  J=JC(L,M)
  SMC=SMO+PHIX(I)*PHIX(J)
  SMT=SMT+PHIT(I)*PHIT(J)
  SMF=SMR+PHIX(I)*PHIT(J)+PHIX(J)*PHIT(I)
  SMC=SMF+PHI(I)*PHI(J)
  IF(MAXSY(M).EQ.0) GC TO 10
  I=IJS(M)
  SMC=SMO+PHIX(I)**2/2.
  SMT=SMT+PHIT(I)**2/2.
  SMR=(SMR+PHIX(I)*PHIT(I))
  SMC=SMF-PHI(I)**2/2.
  GC TO 1C
  CC 21 L=1,MNMAX
  SMC=SMO+PHIX(L)**2
  SMT=SMT+PHIT(L)**2
  SMF=SMF+PHI(L)**2
  IF(N.GT.MNMAXC) GC TO 11
  SMC=SMO+PHIX(M)**2
  SMC=SMO+SMC*.5
  SMT=SMT+SMT*.5
  SMF=SMF+SMF*.5
  SMC=SMF-PHI(M)=0.
  GC TO 9
  CC 10 EX3(N)=SMC
  BT3(N)=SMT

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00011270

EXT3(M)=SMR*.5
BE3(M)=SMF
5 CCNTINUE
RETURN
*****
THIS SECTION HANDLES GENERAL LOADING AND IMPERFECTIONS
*****
1111 CCNTINUE
CC 60 M=1,MNMAX0
KF=K+(M-1)*KMAX
PFX(M)=PHIXB(KP)
FPT(M)=PHITB(KP)
CC 49 M=1,MNMAX
SMC=0.
SMR=0.
SMF=0.
*****
TEST FOR ASYMMETRIC MODE
*****
IF (N(M)-LT.0) GO TO 101
*****
THIS SECTION HANDLES SYMMETRIC MODE COMBINATIONS ONLY
*****
TEST FOR ZERO-TH MCDE
*****
IF (N(M).EQ.0) GO TO 420
MAXL=MAXS(M)
*****
TEST FOR PRESENCE OF SYMMETRIC SLMMATION COMBINATIONS
*****
IF (MAXL.EQ.0) GO TO 42
*****
SET UP -COUPLING- MODES- INDICES AND TEST FOR MODE 1
*****
CC 43 L=1,MAXL
I=JS(L,M)
J=JS(L,M)
II=J-1
JJ=J-1
IF (I.EQ.1) GO TO 43
*****

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C**      CCMPLE SUMS FOR SYMMETRIC SUMMATION COMBINATION MCDES *****00011280
C**      SFC=SMC+PHX(I)*PHX(J)*****00011290
C**      1  +PHX(I)*PHX(J)+PHX(J)*PHX(I)*****00011300
C**      2  -PHX(I)*PHX(J)+PHX(JJ)-PHX(JJ)*PHX(II)*****00011310
C**      1  SMT=SMT-PHT(I)*PHT(J)*****00011320
C**      2  -PHT(I)*PHT(J)-PHT(JJ)+PHT(JJ)*PHT(II)*****00011330
C**      1  +PHX(I)*PHX(J)+PHX(J)*PHX(I)+PHX(I)*PHT(J)*****00011340
C**      2  +PHT(I)*PHT(J)+PHT(JJ)+PHT(JJ)*PHT(II)*****00011350
C**      1  SRR=SMR+PHX(I)*PHX(J)+PHX(J)*PHX(I)*****00011360
C**      2  +PHX(I)*PHX(J)+PHX(J)*PHX(I)+PHX(I)*PHT(J)*****00011370
C**      1  +PHX(J)*PHT(I)*****00011380
C**      2  +PHT(I)*PHT(J)+PHT(JJ)+PHX(JJ)*(PHT(II)*****00011390
C**      3  +PHX(II)*PHT(JJ)+PHX(JJ)*PHT(II)*****00011400
C**      4  SRF=SMF-PHI(I)*PHI(J)*****00011410
C**      1  +PHI(I)*PHI(JJ)*****00011420
C**      2  +PHI(I)*PHI(JJ)*****00011430
C**      3  CCNTINUE*****00011440
C**      4  MAXL=MAXD(N)*****00011450
C**      TEST FOR PRESENCE CF SYMMETRIC DIFFERENCE COMBINATIONS *****00011460
C**      1  IF(MAXL.EQ.0) GO TO 44*****00011470
C**      2  SET UP -COUPLING- MODES- INDICES AND TEST FOR MODE 1 *****00011480
C**      3  *****00011490
C**      4  *****00011500
C**      *****00011510
C**      DC 45 L=1,MAXL*****00011520
C**      1  J=IC(L,M)*****00011530
C**      2  J=JC(L,M)*****00011540
C**      3  II=I-1*****00011550
C**      4  JJ=J-1*****00011560
C**      IF (J.EQ.1) GO TO 442*****00011570
C**      CCMPLE SUMS FOR SYMMETRIC DIFFERENCE COMBINATION MCDES *****00011580
C**      1  SFC=SMC+PHX(I)*PHX(J)*****00011590
C**      2  +PHX(I)*PHX(J)+PHX(JJ)+PHX(JJ)*PHX(II)*****00011600
C**      1  SMT=SMT+PHT(I)*PHT(J)*****00011610
C**      2  +PHT(I)*PHT(J)+PHT(JJ)+PHT(JJ)*PHT(II)*****00011620
C**      1  +PHX(I)*PHX(J)+PHX(J)*PHX(I)*****00011630
C**      2  -PHX(I)*PHX(J)+PHX(JJ)+PHX(JJ)*PHT(II)*****00011640
C**      1  SRR=SMR-PHX(I)*PHX(J)+PHX(J)*PHX(I)*****00011650
C**      2  +PHX(I)*PHX(J)+PHX(J)*PHX(I)+PHX(I)*PHT(J)*****00011660
C**      1  -PHX(I)*PHX(J)+PHX(J)*PHX(I)-PHX(I)*PHT(J)*****00011670
C**      2  +PHX(J)*PHI(I)*****00011680
C**      3  +PHX(II)*PHT(JJ)+PHT(JJ)-PHX(JJ)*(PHT(II)*****00011690
C**      4  +PHI(I)*PHX(JJ)+PHX(JJ)*PHT(II)*****00011700
C**      1  SRF=SMF+PHI(I)*PHI(J)*****00011710
C**      2  +PHI(I)*PHI(JJ)*****00011720
C**      3  GC TO 45*****00011730
C**      4  *****00011740
C**      *****00011750

```


[illegible]


```

C*****
N=AN(MN)
NFS=MASS(K)
CALL BC8(K,B,DB,D,CC)
E(1,1)=B
E(1,2)=C
E(1,3)=0
E(1,4)=C
E(2,1)=C
C1=(1.-NU)
RA=R(K)
GA=GAM(K)
C1=CM1(K)
LEX=DECMX(K)
REX=(3.*QT-0X)
GA2=GA**2
RXE=(3.*QX-0T)
C1X=0T*CX
CNLR=LAM2*D*N*D1/(2.*RA)
CNLR=CNLR*DD/D
E(2,2)=B*D1/2.+LAM2*D*D1*REX**2/8.
E(2,3)=CNLR*REX
E(2,4)=0
E(3,1)=C
E(3,2)=E(2,3)
E(3,3)=LAM2*D*D1*(2.*RAN+(1.+NU)*GA2)
E(3,4)=LAM2
E(4,1)=C
E(4,2)=C
E(4,3)=-D
E(4,4)=C
E(1,1)=GA*B+DB
F(1,2)=(1.+NU)*B*N/(2.*RA)+CNLR*REX*RXE/4.
F(1,3)=B*(0X+NU*0T)+LAM2*D*D1*((1.+NU)*GA2*CX+RAN*RXE/2.)
F(1,4)=LAM2*0X
F(2,1)=-F(1,2)
F(2,2)=(D1/2.)*(GA*B+DB)-(LAM2*C*C1*REX/8.)*(2.*DEX-GA*(5.*0X
1-F(2,3))+LAM2*DD*C1*REX**2/8.
F(2,3)=CNLR*(2.*(1.+NU)*GA*0T-DEX+3.*GA*(CX-CT))+CNLR*REX
F(2,4)=C
F(3,1)=-F(1,3)
F(3,2)=CNLR*(3.*GA*0X-GA*0T*(5.+2.*NU)-DEX)+CNLR*REX
F(3,3)=-LAM2*D*D1*((1.+NU)*GA*0X*0T+GA**3)+2.*GA*RAN)
1+LAM2*CC*D1*((1.+NU)*GA2+2.*RAN)
F(3,4)=LAM2*GA*(2.-NU)
F(4,1)=C*CX
00C14160
00014170
00014180
00014190
00014200
00014210
00014220
00014230
00014240
00014250
00014260
00014270
00014280
00014290
00014300
00014310
00014320
00014330
00014340
00014350
00014360
00014370
00014380
00014390
00014400
00014410
00014420
00014430
00014440
00014450
00014460
00014470
00014480
00014490
00014500
00014510
00014520
00014530
00014540
00014550
00014560
00014570
00014580
00014590
00014600
00014610
00014620
00014630

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```

F(4,2)=0.*NU*GA
F(4,3)=-D.*NU*GA
F(4,4)=0.
G(1,1)=NU*DB*GA-NU*B*OTX-B*GA2-C1*B*GAN/2.-LAM2*D*D1*((1.+NU)*GA2*
1CX*2+RXE**2*GAN/8.)
2.MAS/DELSO
G(1,2)=NU*N*DB/RA-(3.-NU)/(2.*RA)*GA*B*N-CNLR*2.*GA*(REX*RXE/8.
1+(1.+NU)*OTX)
G(1,3)=8*(DEX+GA*(OX-OT))+DB*(OX+NU*OT)-LAM2*C*D1*GA*GAN*(RXE/2.+(
11.+NU)*OX)
G(1,4)=LAM2*D1*GA*CX
G(2,1)=-B*GAN*(3.-NU)/(2.*RA)-D1*N*DB/(2.*RA)+DNLR*2.*(-1.*(1.+
1NU)*GA*CTX+GA/8.*(6.*OTX-7.*OX**2-3.*OT**2)-DEX/4.*(5.*CT-3.*CX))
2-CNLR/4.*REX*RXE
G(2,2)=-GA*F(2,2)+D1/2.*B*OTX-B*GAN-LAM2*D*C*D1*((1.+NU)*CT**2*GAN
1-CTX/8.*REX**2)
2.MAS/DELSO
G(2,3)=-B*N*(OT+NU*OX)/RA+DNLR*(GA*DEX-2.*GA2*OX-2.*(1.+NU)*CT
1*GAN+REX*(GA2+OTX))-DNLR*REX*GA
G(2,4)=-NU*LAM2*OT*N/RA
1-CX*GAN+2.*OTX*CX)+GAN/2.*(GA*CX-CA*OT-3.*DEX))
2-LAM2*CC*D1*((1.+NU)*GA2*OX+GAN/2.*RXE)
G(2,2)=-B*N*(OT+NU*CX)/RA+DNLR*(2.*(1.+NU)*GA2
1*CT-OT*GAN)+GA*DEX+3.*GA2*(CT-OX)+CTX*REX*(2.*(1.+NU)*GA
2*CT+GA*REX)
G(2,3)=-B*(OX**2+2.*NU*OTX+OT**2)+LAM2*DD*D1*GAN*(3.+NU)*GA
1+2.*GA2)+2.*(GA2+CTX))-LAM2*DD*D1*GAN*(3.+NU)*GA
2.MAS/DELSO
G(2,4)=-LAM2*(D1*CTX+NU*GAN)
G(4,1)=C*(DEX+NU*GA*OX)
G(4,2)=C*NU*OT/RA
G(4,3)=C*NU*GAN
G(4,4)=-1.
RETURN
END
SLEROUTINE POLE(K,P,DEE,DST,X,Z,ZO,Z2,Z3,ZDCT,IS,JS,ID,JD,PHIXB,
1PFI1B)
C*****
C*****THIS SUBROUTINE PRINTS THE SOLUTION AT AN INITIAL *
C*****PCLE.
C*****
C*****INFLICIT LCGICAL*1 ($)
C*****REAL NU,MT,MX,MTH,MXT,MIS,KX,KT,KXT,LAM,LAM2,MASS
C*****DIMENSION P(4,4,1),DEE(4,4,1),DST(4,4,1),X(4,1),Z(4,1),ZC(4,1),
1Z2(4,1),Z3(4,1),ZDCT(4,1),IS(99,1),JS(99,1),ID(99,1),JD(99,1),
2PFI1B(1),PFI1B(1)
C(CMNON / IBL2/ N(99),MNINIT
00014640
00014650
00014660
00014670
00014680
00014690
00014700
00014710
00014720
00014730
00014740
00014750
00014760
00014770
00014780
00014790
00014800
00014810
00014820
00014830
00014840
00014850
00014860
00014870
00014880
00014890
00014900
00014910
00014920
00014930
00014940
00014950
00014960
00014970
00014980
00014990
00015000
00015010
00015020
00015030
00015040
00015050
00015060
00015070
00015080
00015090
00015100
00015110

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CCMMCN /IBL3/ MO,M1,M2,M3
CCMMCN /IBL4/ KMAX,KL,IBCFNL
CCMMCN /IBL5/ IBCINL,MAXD(99),MAXS(59),MAXSY(99),IJS(59)
CCMMCN /IBL7/ MNMAXO,MAXD(99),MAXS(59),MAXSY(99),IJS(59)
CCMMCN /IBL8/ LSTEP,ITR
CCMMCN /IBL10/ IFREQ,NTHMAX
CCMMCN /IBL12/ KMAX1,KMAX2,NCONV
CCMMCN /IBLJ/ JUMP
CCMMCN /IBL4/ ZFLM(4,4,59),ZF2M(4,4,99),
1 ZF3M(4,4,59),ZF4M(4,4,99),
TT(99),MT(99),DT(99),DMT(95)
CCMMCN /BL5/ SOE,CSE,ALOAD
CCMMCN /BL6/ DI,SI
CCMMCN /BL7/ R(500),GAM(500),CMT(500)
CCMMCN /BL10/ PHIX(59),PHIT(99),PHI(99)
CCMMCN /BL11/ OMXI(500),PHEE,T0,T2
CCMMCN /BL11A/ PHEN,I2N
CCMMCN /BL12/ TDLI,IDEI
CCMMCN /BL14/ LAM2,LSD18,LSD1N
CCMMCN /BL15/ NU,U1(99),V1(99),W1(99),V2(99),U2(99),W2(99),U3(99),
1 V3(99),W3(99)
CCMMCN /BL17/ DEL(36)
CCMMCN /BL19/ TH(36)
CCMMCN /BL20/ DEOMX(500)
CCMMCN /BL27/ BX3(59),BXT3(99),BE3(59)
CCMMCN /BL31/ DELSQ,EXTI(99)
CCMMCN /BL32/ TKN,ELAST,CHAR,SIGC
CCMMCN /BL100/ TEEC,$DYNMC
CCMMCN /BL101/ DELSO
CCMMCN /BL102/ DELCAD
CCMMCN /BL103/ MASS(500)
CCMMCN /BL110/ TX(99),TTH(99),TXT(99),MX(55),MTH(59),MXT(59),
1 QS(99)
CCMMCN /BL111/ ABZ,ABZO,ABZN,ABZ3,DD2
C*****
CALL BCR(K,BS,DB,CS,DD)
M1=M1-1
M2=M2-1
IF(K.EQ.KMAX) GO TO 301
CC 202 MN=1,MNMAXO
V1(MN)=L2(MN)
V1(MN)=V2(MN)
W1(MN)=W2(MN)
I3=3+(MN-1)*KMAX2
I2=I3-1
I2(MN)=Z(1,I3)
V2(MN)=Z(2,I3)
W2(MN)=Z(3,I3)

```



```

FFIX(MN)=0.0
FFIT(MN)=0.0
PFIT(MN)=0.0
MX(MN)=Z(4,I2)*ABZ3
MTF(MN)=0.0
MXT(MN)=0.0
CS(MN)=0.0
TX(MN)=0.0
TTF(MN)=0.0
TIT(MN)=0.0
IF(M1.EQ.0) GO TO 203
CALL INLPCL(Z,PHIX8,PHIT8)
FFIX(M1)=PFEE*ABZ0
PFIT(M1)=-PHEE*ABZC
IF(JUMP.EQ.1) GO TC 1001
PFIX(M1L)=PHEN*ABZ0
FFIT(M1L)=PHIX(M1L)
CCNTINUE
II=3+(M1-1)*KMAX2
IF1=II+1
IM1=II-1
GA2=GAM(2)
CALL BCR(2,BS,DB,CS,DD)
CALL TLCAD(2,Z)
PFIXX=-Z(3,II)/R(2)+CMT(2)*Z(2,II)*Z(1,II)
PFITT=Z(3,II)/R(2)-Z(2,IM1)*TCL1+GA2*Z(2,II)/R(2))/2.
CS(M1)=(SIGO*TKN*LAM2*((2.-NU)*Z(4,II)-DS*CC2*(PHITT/R(2)+PHIXX/R(2)-CMT(2)-CMT(2)))+D1*MT(M1)*ALOAD+DS*D1*(-PHIXX/R(2)-GA2*PHITT+(CMT(2)-CMT(2)))*Z(2,II)+CMT(2)*(Z(2,II)-Z(2,IM1))*TDL1)*.5)/CEL
1 IF(MO.EQ.0) GO TO 204
2 IXX(MO)=IO*ABZ
3 TTF(MO)=IO*ABZ
MTF(MO)=MX(MO)
IF(M2.EQ.0) GO TC 205
TIX(M2)=T2*ABZ
TIT(M2)=-T2*ABZ
TXT(M2)=-T2*ABZ
MTF(M2)=-MX(M2)
MXT(M2)=MTH(M2)
IF(JUMP.EQ.1) GO TC 205
TIX(M2L)=T2N*ABZ
TIT(M2L)=-TIX(M2L)
TXT(M2L)=TIX(M2L)
MXT(M2L)=-MX(M2L)
GC TO 205
2C2
2C4
10C1

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```

2C3 IF(MO.EQ.0) GO TO 206
I3=3+(MC-1)*KMAX2
I4=I3+1
CALL LQAD(1,Z)
TX(MO)=BS*SI*((2.*Z(1,I3)-.5*Z(1,I4))/DEL+OMXI(1)*Z(3,I3-1))*ABZ
1 TX(MO)=TX(MO)
MTF(MO)=MX(MO)
2C6 IF(M2.EC.0) GO TO 205
I3=3+(M2-1)*KMAX2
I4=I3+1
TX(M2)=BS*D1*(2.*Z(1,I3)-.5*Z(1,I4))/DEL
TX(M2)=TX(M2)*ABZ
TX(M2)=-TX(M2)
TX(M2)=-TX(M2)
MTF(M2)=-MX(M2)
MX(M2)=-MX(M2)
IF(JUMP.EQ.1) GO TO 205
TX(M2L)=BS*D1*(2.*Z(1,I3-KMAX2)-.5*Z(1,I4-KMAX2))/DEL
TX(M2L)=TX(M2L)*ABZ
TX(M2L)=-TX(M2L)
TX(M2L)=TX(M2L)
MTF(M2L)=-MX(M2L)
MX(M2L)=MX(M2L)
RETURN
3C1 CCNTINUE
CC 302 MN=1,MNMAXC
LI(MN)=L2(MN)
V1(MN)=V2(MN)
W1(MN)=W2(MN)
PFI(MN)=0.
PFI(MN)=0.
PFI(MN)=0.
IK=KMAX1+(MN-1)*KMAX2
M(MN)=Z(4,IK)*ABZ3
MTF(MN)=0.
MX(MN)=0.
CS(MN)=C.
TX(MN)=C.
TX(MN)=0.
TX(MN)=0.
IF(M1.EC.0) GO TO 303
CALL FNLPC(LZ,PHIXB,PHITB)
PFI(M1)=PTEE*ABZC
PFI(M1)=PHEE*ABZC
IF(JUMP.EQ.1) GO TO 1002
PFI(M1L)=PHEN*ABZC
PFI(M1L)=-PHIX(M1L)

```



```

10C2 CCNTINUE
      II=KMAX+(M1-1)*KMAX2
      IF I=II+1
      IM1=II-1
      GAK=GAM(KL)
      CALL BCB(KL,BS,DB,DS,DD)
      CALL TLCD(KL,Z)
      PFIIX=Z(3,IM1)*TDLI+OMXI(KL)*Z(1,II)
      PFIIT=Z(3,II)/R(KL)+OMT(KL)*Z(2,II)
      PFII=((Z(2,IP1)-Z(2,IM1))*TDLI+GAK*Z(2,II)+Z(1,II)/R(KL))/2.
      CS(M1)=-SIGO*TKN*LAM2*((2.-NU)*Z(4,II)-DS*DC2*(PHIIT/R(KL))+PFIIX
1*GAK)+C1*MT(M1)*ALCAC-DS*D1*(-PFIIX/R(KL)-GAK*PHIIT+(OMT(KL)-OMXI
2(KL))*PHIIT+(-Z(3,IM1)*TDLI-GAK*Z(3,II))/R(KL)+GAK*(CMXI(KL)
3-OMT(KL))*Z(2,II)+CMT(KL))*Z(2,IM1))*TDLI)*.5)
4/DEL
      IF(MO.EQ.0) GO TO 304
      TX(MO)=TO*ABZ
      TTH(MO)=TO*ABZ
      TTF(MO)=MX(MO)
304 IF(M2.EC.0) GO TO 305
      TX(M2)=T2*ABZ
      TTF(M2)=-T2*ABZ
      TX1(M2)=T2*ABZ
      MTF(M2)=-MX(M2)
      MXT(M2)=MX(M2)
      IF(JUMP.EQ.0) GO TC 305
      TX(M2L)=T2N*ABZ
      TTF(M2L)=-TX(M2L)
      TX1(M2L)=-TX(M2L)
      MTF(M2L)=-MX(M2L)
      MXT(M2L)=-MX(M2L)
      GC TO 305
303 IF(MO.EQ.0) GO TO 306
      IKM=KMAX+(MO-1)*KMAX2
      IM1=IKM-1
      CALL TLCD(KMAX,Z)
      TX(MO)=BS*SI*(-2.*Z(1,IKM)+.5*Z(1,IM1))/DEL+CMXI(KMAX)*Z(3,IKM+1)
1)*ABZ-TT(MC)*ABZ*ALCAD
      TTF(MO)=TX(MO)
      MTF(MO)=MX(MO)
      IF(M2.EC.0) GO TO 305
      IKM=KMAX+(M2-1)*KMAX2
      IM1=IKM-1
      TX(M2)=BS*D1*(-2.*Z(1,IKM)+.5*Z(1,IM1))/DEL
      TX1(M2)=TX(M2)*ABZ
      TTF(M2)=-TX(M2)
      TX1(M2)=TX(M2)
      MTF(M2)=-MX(M2)

```



```

C ** SET UP THIRD LOOP - TC COMPARE SUM WITH ALL OTHER MCDES ** 00018480
C ** CC 302 MMFT=1,MNMAX,JUMP ** 00018490
C ** IF WE SATISFY HERE, MODE EXISTS, GC TO INCREMENT -MAXS- CR ** 00018500
C ** -MAXSY-) ** 00018510
C ** IF(NTTEST.EQ.N(MMFT)) GC TO 310 ** 00018520
C ** 302 CCNTINUE ** 00018530
C ** IF WE MAKE IT TO HERE, WE HAVE GENERATED A NEW MCDE ** 00018540
C ** CC WE WANT ANY MORE NEW MODES ** 00018550
C ** IF(ICORFL.EQ.1) GC TO 301 ** 00018560
C ** IF(MNMAX.GE.MAXM) GC TO 301 ** 00018570
C ** INCREMENT -MNMAX- AND ESTABLISH NEW MODE NUMBER ** 00018580
C ** MNMAX=MNMAX+JUMP ** 00018590
C ** N(MNMAX)=NTEST ** 00018600
C ** IF(JUMP.GT.1) N(MNMAX-1)=-NTEST ** 00018610
C ** IF(MNMAX.GE.MAXM) ICORFL=1 ** 00018620
C ** IF MCDE WAS ADDED TO ITSELF, GO TC -MAXSY AND IJS- SECTICN ** 00018630
C ** 31C IF(MNMAX.EQ.NMM) GC TC 360 ** 00018640
C ** MAKE ENTRIES IN -LOCS-, -IS- AND -JS- ** 00018650
C ** LCCS=MAXS(MMFT)+1 ** 00018660
C ** MAXS(MMFT)=LOCS ** 00018670
C ** IJS(LOCS,MMFT)=MN ** 00018680
C ** JS(LOCS,MMFT)=MM ** 00018690
C ** GC TO 301 ** 00018700
C ** SEE IF THE SUM OF THE MCDE WITH ITSELF WAS THE 0-TH MCDE ** 00018710
C ** 36C IF(MNMAX.EQ.C) GC TO 301 ** 00018720
C ** IF HERE, IT WASN-T, MAKE ENTRIES IN -MAXSY- AND -IJS- ** 00018730
C ** MAXSY(MMFT)=1 ** 00018740
C ** IJS(MMFT)=MN ** 00018750
C ** CCNTINUE ** 00018760
C ** MNINIT=MNMAX+JUMP ** 00018770
C ** IF(ICORFL.GT.0) IPASS=IPASS+1 ** 00018780
C ** ** 00018790
C ** ** 00018800
C ** ** 00018810
C ** ** 00018820
C ** ** 00018830
C ** ** 00018840
C ** ** 00018850
C ** ** 00018860
C ** ** 00018870
C ** ** 00018880
C ** ** 00018890
C ** ** 00018900
C ** ** 00018910
C ** ** 00018920
C ** ** 00018930
C ** ** 00018940
C ** ** 00018950

```



```

IF(IPASS.LT.2.AND.MNINIT.LE.MNMAX) CALL PMATRIX (P,X,ZC,Z2,Z3,ZEE,
1CST)
RETURN
END
SUBROUTINE TEAETA(K,Z,IS,JS,ID,JC)
C*****
C THIS SUBROUTINE CALCULATES THE INPLANE FORCES AND CARRIES CUT
C THE MULTIPLYING AND SUMMATION PROCEDURE FOR COMPUTING THE ETA
C NCN-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
C IS, ID, JS, IJS, MAXS, MAXC, MAXSY PREFARED IN SUBROUTINE
C MODES ARE USED HERE
C*****
C*****
REAL NU,MT
DIMENSION Z(4,1),IS(95,1),JS(99,1),ID(95,1),JC(99,1)
COMMON /IBL1/ MNMAX
COMMON /IBL2/ N(95),MNINIT
COMMON /IBL7/ MNMAXO,MAXD(99),MAXS(99),MAXSY(99),IJS(99)
COMMON /IBL8/ LSTEP,ITR
COMMON /IBL13/ ITRMAX,LSEXMAX
5/IBLJ/ JUMP
COMMON /BL5/ TT(99),MT(99),DT(95),DMT(99)
COMMON /BL6/ SOE,CSE,ALOAD
COMMON /BL7/ D1,S1
COMMON /BL8/ R(500),GAM(500),DMT(500)
COMMON /BL10/ PHIX(99),PHIT(99),PHI(99)
COMMON /BL11/ QMXI(500),PHEE,T0,T2
COMMON /BL12/ TDLI,TDEL
COMMON /BL15/ NU,UI(99),V1(99),V2(99),V3(99),U2(99),U3(99),
1 CCMMGN /BL27/ BX3(99),BT3(99),BXT3(99),BE3(99)
CCMMGN /BL28/ EXX3(99),ETX3(99),ETX3(99),ET3(99)
CCMMGN /BLPHS/ PHX(99),PHT(99)
C DIMENSION ICN TX(99),TTH(99),TXI(99)
C*****
C*****
RRA=1./R(K)
GA=GAM(K)
CX=CMXI(K)
CT=GMT(K)
CALL BCE(K,BS,DB,CS,DD)
DC 1 N=1,MNMAXO
PHIX(M)=PHIX(M)+PHX(M)
PHT(M)=PHT(M)+PHT(M)
EN=N(M)
CALL TLGAD(K,Z)
TTS=TT(M)-UL(M)
EX=(U3(M)-UI(M))*TDLI+OX*W2(M)+CSE*(BX3(M)+EE3(M))
ET=EN*V2(M)*RRA+GA*U2(M)+OT*W2(M)+OSE*(BT3(M)+BE3(M))
EXT=.5*(TDLI*(V3(M)-V1(M))-EN*U2(M)*RRA-GA*V2(M))+CSE*EXT3(M)
C*****
00018960
00018970
00018980
00018990
00019000
00019010
00019020
00019030
00019040
00019050
00019060
00019070
00019080
00019090
00019100
00019110
00019120
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00019370
00019380
00019390
00019400
00019410
00019420
00019430

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TX(M)=BS*(EX+NU*ET)-TTS
TTH(M)=BS*(ET+NU*EX)-TTS
TXI(M)=BS*CI*EXT
1 IF(JUMP.EQ.2) GO TC 1111
CC 9 N=1,MNMAX
SMF=0.
SMV=0.
SME=0.
SMN=0.
SMI=0.
IF(N(M).EQ.0) GO TC 20
MAXL=MAXS(M)
IF(MAXL.EQ.0) GO TO 2
CC 3 L=1,MAXL
I=IS(L,M)
J=JS(L,M)
SMF=SMF+TX(I)*PHIX(J)+TX(J)*PHIX(I)
SMV=SMV+TTH(I)*PHIT(J)+TTH(J)*PHIT(I)
SME=SMV-PHIT(I)*TXI(J)-PHIT(J)*TXI(I)
SMN=SMN+PHIX(I)*TXI(J)+PHIX(J)*TXI(I)
SMI=SMI+TX(I)*PHI(J)+TX(J)*PHI(I)
SMX=SMX+TTH(I)*PHI(J)+TTH(J)*PHI(I)
3 IF(MAXL.EQ.0) GO TO 4
CC 5 L=1,MAXL
I=IC(L,M)
J=JC(L,M)
SMF=SMF+TX(I)*PHIX(J)+TX(J)*PHIX(I)
SMV=SMV-TTH(I)*PHIT(J)+TTH(J)*PHIT(I)
SME=SMV-PHIT(I)*TXI(J)+PHIT(J)*TXI(I)
SMN=SMN-PHIX(I)*TXI(J)+PHIX(J)*TXI(I)
SMI=SMI-TTH(I)*PHI(J)+TTH(J)*PHI(I)
5 IF(MAXSY(M).EQ.0) GO TC 10
I=IS(M)
SMF=SMF+TX(I)*PHIX(I)
SMV=SMV+TTH(I)*PHIT(I)
SME=SMV-PHIT(I)*TXI(I)
SME=SMV-PHIX(I)*TXI(I)
SMN=SMN+TX(I)*PHI(I)
SMI=SMI+TTH(I)*PHI(I)
6 CC 21 L=1,MNMAX
SMF=SMF+TX(L)*PHIX(L)
SMV=SMV+PHIT(L)*TXI(L)
21 IF(M.GT.MNMAX) GO TO 10
SMF=SMF+TX(M)*PHIX(M)

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```

00C19440
00019450
00019460
00019470
00019480
00C19490
00C19500
00C19510
00C19520
00C19530
00019540
00C19550
00C19560
00019570
00C19580
00019590
00C19600
00C19610
00019620
00C19630
00C19640
00C19650
00C19660
00C19670
00019680
00019690
00019700
00019710
00C19720
00019730
00C19740
00019750
00019760
00019770
00C19780
00019790
00C19800
00C19810
00019820
00C19830
00C19840
00C19850
00019860
00019870
00C19880
00019890
00C19900
00C19910

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C *** CCMPLE SUMS FOR ASYMMETRIC DIFFERENCE COMBINATIONS *** 00021840
C *** SMF=SMF-P+IX(I)*TX(JJ)+PHIX(J)*TX(II)+PHIX(II)*TX(J) *** 00021850
1 *** -PHIX(JJ)*TX(I) *** 00021860
1 *** +PHIT(JJ)*TTH(I) *** 00021870
1 *** +PHIT(JJ)*TTH(II)+PHIT(II)*TTH(J) *** 00021880
1 *** +PHIT(JJ)*TX(I) *** 00021890
1 *** +PHIT(JJ)*TX(II)+PHIT(II)*TX(J) *** 00021900
1 *** +PHIX(JJ)*TX(I) *** 00021910
1 *** +PHIX(JJ)*TX(II)+PHIX(II)*TX(J) *** 00021920
1 *** +PHIX(JJ)*TX(I) *** 00021930
1 *** +PHIX(JJ)*TX(II)+PHI(II)*TX(J) *** 00021940
1 *** +PHI(JJ)*TX(I) *** 00021950
1 *** +PHI(JJ)*TTH(I) *** 00021960
1 *** +PHI(JJ)*TTH(II)+PHI(II)*TTH(J) *** 00021970
1 *** GC TO 1C5 *** 00021980
C *** EXECUTE BELOW IF J=1 IN DIFF-COMB (OR I=1 IN SUM-COMB) *** 00021990
C *** SMF=SMF+(PHIX(I)*TX(II)+PHIX(II)*TX(I))*2.0 *** 00022000
123 *** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022010
*** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022020
*** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022030
*** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022040
*** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022050
*** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022060
1C5 *** SPS=SPS+(PHIT(I)*TTH(I)+PHIT(II)*TTH(II))*2.0 *** 00022070
C *** CCNTINUE *** 00022080
C *** TEXT FOR PRESENCE CF SAME-INDEX COMBINATION *** 00022090
C *** 1C4 IF (MAXSY(MP).EQ.0) GC TO 410 *** 00022100
C *** SET UP COUPLING MCDSES- INDICES AND COMPILE SUMS *** 00022110
C *** I=IJS(MP) *** 00022120
C *** I=I-1 *** 00022130
C *** SMF=SMF+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022140
C *** SPS=SPS+PHIT(I)*TTH(II)+PHIT(II)*TTH(I) *** 00022150
C *** SPS=SPS+PHIT(I)*TTH(II)+PHIT(II)*TTH(I) *** 00022160
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022170
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022180
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022190
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022200
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022210
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022220
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022230
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022240
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022250
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022260
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022270
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022280
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022290
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022300
C *** SPS=SPS+PHIX(I)*TX(II)+PHIX(II)*TX(I) *** 00022310

```


APPENDIX B

LISTING OF OUTPUT FROM EXAMPLE PROBLEM

1000 TEST CASE, INDICATIVELY LEADING CASE

--INPUT DATA RECORD--

THE BOUNDARY CONDITIONS ARE:

AT THE INITIAL EDGE

--MEGA BAR--				--LAMB BAR--			
(C.0	0.0	0.0	C.0	(0.100E 01	0.0	0.0	0.0
(0.0	0.0	0.0	0.0	(0.0	0.100E 01	0.0	0.0
(0.0	0.0	0.0	0.0	(0.0	0.0	0.100E 01	0.0
(0.0	0.0	0.0	0.100E 01	(0.0	0.0	0.0	0.0

AT THE FINAL EDGE

--MEGA BAR--				--LAMB BAR--			
(0.0	0.0	0.0	0.0	(0.100E 01	0.0	0.0	0.0
(0.0	0.0	0.0	0.0	(0.0	0.0	0.0	0.0
(0.0	0.0	0.0	0.0	(0.0	0.0	0.0	0.0
(0.0	0.0	0.0	0.100E 01	(0.0	0.0	0.0	0.0

NUMBER OF STATIONS----- 31
 NUMBER OF MODES----- 4
 INCREMENTAL TIME----- .1024E-01
 MAXIMUM NUMBER OF TIME STEPS----- 750
 MAXIMUM NUMBER OF ITERATIONS----- 20
 CONVERGENCE CRITERION----- 0.0100

CHARACTERISTIC SHELL DIMENSION----- 0.1500E 02
 REFERENCE THICKNESS----- 0.5430E 00
 REFERENCE ELASTICITY----- 0.3530E 07
 REFERENCE STRESS----- 0.1030E 04
 REFERENCE TIME----- 0.1046E-03
 POISSON'S RATIO----- 0.2060E 01

CIRCUMFERENTIAL COORDINATES FOR THE PRINT RECORD, IN RADIAN MEASURE, ARE:

0.0 3.141592054

THE DATA PRINTED IS DIMENSIONAL
 EXECUTING IN SUBROUTINE "MORPHAT"

STATION	RADIUS	GAUSS	CPGA S	OPCA DIFFA	DEFFCA S	MASS
1	0.7920E 01	0.1012E-01	0.0	0.1243E 00	0.0	0.1021E-03
2	0.8026E 01	0.1076E-01	0.0	0.1241E 00	0.0	0.1021E-03
3	0.8102E 01	0.1176E-01	0.0	0.1220E 00	0.0	0.1021E-03
4	0.8178E 01	0.1250E-01	0.0	0.1209E 00	0.0	0.1021E-03
5	0.8264E 01	0.1335E-01	0.0	0.1197E 00	0.0	0.1021E-03
6	0.8340E 01	0.1425E-01	0.0	0.1187E 00	0.0	0.1021E-03
7	0.8406E 01	0.1508E-01	0.0	0.1176E 00	0.0	0.1021E-03
8	0.8468E 01	0.1595E-01	0.0	0.1165E 00	0.0	0.1021E-03
9	0.8534E 01	0.1675E-01	0.0	0.1154E 00	0.0	0.1021E-03
10	0.8604E 01	0.1758E-01	0.0	0.1143E 00	0.0	0.1021E-03
11	0.8676E 01	0.1839E-01	0.0	0.1132E 00	0.0	0.1021E-03
12	0.8750E 01	0.1923E-01	0.0	0.1121E 00	0.0	0.1021E-03
13	0.8826E 01	0.2008E-01	0.0	0.1110E 00	0.0	0.1021E-03
14	0.8904E 01	0.2094E-01	0.0	0.1099E 00	0.0	0.1021E-03
15	0.8984E 01	0.2181E-01	0.0	0.1087E 00	0.0	0.1021E-03
16	0.9066E 01	0.2269E-01	0.0	0.1075E 00	0.0	0.1021E-03
17	0.9150E 01	0.2358E-01	0.0	0.1063E 00	0.0	0.1021E-03
18	0.9236E 01	0.2448E-01	0.0	0.1051E 00	0.0	0.1021E-03
19	0.9324E 01	0.2539E-01	0.0	0.1039E 00	0.0	0.1021E-03
20	0.9414E 01	0.2631E-01	0.0	0.1027E 00	0.0	0.1021E-03
21	0.9506E 01	0.2724E-01	0.0	0.1015E 00	0.0	0.1021E-03
22	0.9599E 01	0.2818E-01	0.0	0.1003E 00	0.0	0.1021E-03
23	0.9694E 01	0.2913E-01	0.0	0.0991E 00	0.0	0.1021E-03
24	0.9790E 01	0.3009E-01	0.0	0.0979E 00	0.0	0.1021E-03
25	0.9887E 01	0.3106E-01	0.0	0.0967E 00	0.0	0.1021E-03
26	0.9986E 01	0.3204E-01	0.0	0.0955E 00	0.0	0.1021E-03
27	1.0086E 01	0.3303E-01	0.0	0.0943E 00	0.0	0.1021E-03
28	1.0187E 01	0.3403E-01	0.0	0.0931E 00	0.0	0.1021E-03
29	1.0289E 01	0.3504E-01	0.0	0.0919E 00	0.0	0.1021E-03
30	1.0392E 01	0.3606E-01	0.0	0.0907E 00	0.0	0.1021E-03
31	1.0496E 01	0.3709E-01	0.0	0.0895E 00	0.0	0.1021E-03

STATION	P STIFFNESS	D STIFFNESS	B PRIME	D PRIME
1	0.208163E 07	0.511471E 05	0.0	0.0
2	0.208163E 07	0.511471E 05	0.0	0.0
3	0.208163E 07	0.511471E 05	0.0	0.0
4	0.208163E 07	0.511471E 05	0.0	0.0
5	0.208163E 07	0.511471E 05	0.0	0.0
6	0.208163E 07	0.511471E 05	0.0	0.0
7	0.208163E 07	0.511471E 05	0.0	0.0
8	0.208163E 07	0.511471E 05	0.0	0.0
9	0.208163E 07	0.511471E 05	0.0	0.0
10	0.208163E 07	0.511471E 05	0.0	0.0
11	0.208163E 07	0.511471E 05	0.0	0.0
12	0.208163E 07	0.511471E 05	0.0	0.0
13	0.208163E 07	0.511471E 05	0.0	0.0
14	0.208163E 07	0.511471E 05	0.0	0.0
15	0.208163E 07	0.511471E 05	0.0	0.0
16	0.208163E 07	0.511471E 05	0.0	0.0
17	0.208163E 07	0.511471E 05	0.0	0.0
18	0.208163E 07	0.511471E 05	0.0	0.0
19	0.208163E 07	0.511471E 05	0.0	0.0
20	0.208163E 07	0.511471E 05	0.0	0.0
21	0.208163E 07	0.511471E 05	0.0	0.0
22	0.208163E 07	0.511471E 05	0.0	0.0
23	0.208163E 07	0.511471E 05	0.0	0.0
24	0.208163E 07	0.511471E 05	0.0	0.0
25	0.208163E 07	0.511471E 05	0.0	0.0
26	0.208163E 07	0.511471E 05	0.0	0.0
27	0.208163E 07	0.511471E 05	0.0	0.0
28	0.208163E 07	0.511471E 05	0.0	0.0
29	0.208163E 07	0.511471E 05	0.0	0.0
30	0.208163E 07	0.511471E 05	0.0	0.0
31	0.208163E 07	0.511471E 05	0.0	0.0

THE INITIAL CONDITIONS FOR N = 0 FOLLOW

STATION	U	V	W	S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U	V	W	S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE INITIAL CONDITIONS FOR N= 1 FOLLOW

STATION	U	V	W	M S
1	0.0	1.0	0.0	0.0
2	0.0	1.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DET	V DET	W DET	M S DET
1	0.0	0.0	0.0	0.0
2	0.0	0.0	-0.222040E 04	0.0
3	0.0	0.0	-0.222040E 04	0.0
4	0.0	0.0	-0.222040E 04	0.0
5	0.0	0.0	-0.222040E 04	0.0
6	0.0	0.0	-0.222040E 04	0.0
7	0.0	0.0	-0.222040E 04	0.0
8	0.0	0.0	-0.222040E 04	0.0
9	0.0	0.0	-0.222040E 04	0.0
10	0.0	0.0	-0.222040E 04	0.0
11	0.0	0.0	-0.222040E 04	0.0
12	0.0	0.0	-0.222040E 04	0.0
13	0.0	0.0	-0.222040E 04	0.0
14	0.0	0.0	-0.222040E 04	0.0
15	0.0	0.0	-0.222040E 04	0.0
16	0.0	0.0	-0.222040E 04	0.0
17	0.0	0.0	-0.222040E 04	0.0
18	0.0	0.0	-0.222040E 04	0.0
19	0.0	0.0	-0.222040E 04	0.0
20	0.0	0.0	-0.222040E 04	0.0
21	0.0	0.0	-0.222040E 04	0.0
22	0.0	0.0	-0.222040E 04	0.0
23	0.0	0.0	-0.222040E 04	0.0
24	0.0	0.0	-0.222040E 04	0.0
25	0.0	0.0	-0.222040E 04	0.0
26	0.0	0.0	-0.222040E 04	0.0
27	0.0	0.0	-0.222040E 04	0.0
28	0.0	0.0	-0.222040E 04	0.0
29	0.0	0.0	-0.222040E 04	0.0
30	0.0	0.0	-0.222040E 04	0.0
31	0.0	0.0	-0.222040E 04	0.0

THE INITIAL CONDITIONS FOR $n = 2$ FOLLOW

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DOT	V DOT	W DOT	M S DOT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	-0.942366E 03	0.0
3	0.0	0.0	-0.942366E 03	0.0
4	0.0	0.0	-0.942366E 03	0.0
5	0.0	0.0	-0.942366E 03	0.0
6	0.0	0.0	-0.942366E 03	0.0
7	0.0	0.0	-0.942366E 03	0.0
8	0.0	0.0	-0.942366E 03	0.0
9	0.0	0.0	-0.942366E 03	0.0
10	0.0	0.0	-0.942366E 03	0.0
11	0.0	0.0	-0.942366E 03	0.0
12	0.0	0.0	-0.942366E 03	0.0
13	0.0	0.0	-0.942366E 03	0.0
14	0.0	0.0	-0.942366E 03	0.0
15	0.0	0.0	-0.942366E 03	0.0
16	0.0	0.0	-0.942366E 03	0.0
17	0.0	0.0	-0.942366E 03	0.0
18	0.0	0.0	-0.942366E 03	0.0
19	0.0	0.0	-0.942366E 03	0.0
20	0.0	0.0	-0.942366E 03	0.0
21	0.0	0.0	-0.942366E 03	0.0
22	0.0	0.0	-0.942366E 03	0.0
23	0.0	0.0	-0.942366E 03	0.0
24	0.0	0.0	-0.942366E 03	0.0
25	0.0	0.0	-0.942366E 03	0.0
26	0.0	0.0	-0.942366E 03	0.0
27	0.0	0.0	-0.942366E 03	0.0
28	0.0	0.0	-0.942366E 03	0.0
29	0.0	0.0	-0.942366E 03	0.0
30	0.0	0.0	-0.942366E 03	0.0
31	0.0	0.0	-0.942366E 03	0.0

144 INITIAL CONDITIONS FOR M= 4 FOLLOW

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DOT	V DOT	W DOT	M S DOT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.0

STATION	N S	N THETA	M	M THETA	Q S	PHI	PHI THETA	M S	M THETA	N THETA
1	-0.3459E-04	-0.9571E-03	0.0	-0.2372E-04	-0.2372E-04	0.0	0.2386E-03	0.5824E-02	0.0	0.0
14	0.7629E-03	0.2651E-04	0.0	0.2531E-04	0.2531E-04	0.0	0.1838E-04	0.6549E-03	0.0	0.0
27	0.3078E-04	-0.3224E-04	0.0	0.2360E-04	0.2360E-04	0.0	-0.6158E-03	-0.1716E-03	0.0	0.0
31	0.2021E-04	0.7875E-03	0.0	0.1122E-04	0.1122E-04	0.0	-0.9756E-02	-0.2790E-02	0.0	0.0

PHI

PHI THETA

PHI S

M

V

STATION

PHI S

M

V

STATION

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.016159E-01

STATION	N S	N THETA	M	M THETA	Q S	PHI	PHI THETA	M S	M THETA	N THETA
1	-0.4580E-04	-0.1275E-04	-0.3960E-02	-0.1933E-04	-0.1933E-04	0.0	0.1454E-04	0.4150E-03	-0.1914E-04	0.0
14	0.6554E-04	-0.3791E-05	-0.1549E-02	-0.2551E-04	-0.2551E-04	0.0	-0.8058E-03	-0.3320E-03	0.1056E-03	0.0
27	-0.3588E-04	-0.6111E-04	0.4616E-02	0.3540E-04	0.3540E-04	0.0	0.8024E-03	0.1065E-03	-0.7260E-04	0.0
31	-0.1638E-04	-0.5050E-03	0.3203E-02	0.5999E-04	0.5999E-04	0.0	0.1458E-04	0.4284E-03	0.1160E-04	0.0

PHI

PHI THETA

PHI S

M

V

STATION

PHI

PHI THETA

PHI S

M

V

STATION

APPENDIX C

INPUT DATA GUIDE FOR SATANS-IIA

INPUT DATA GUIDE FOR SATANS-I, SATANS-II, AND SATANS-IIA

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
1	1-72	18A4	TITLE	-	ENTER ANY 72 CHARACTERS
2	1-5	I5	NO	1	THE PROBLEM NUMBER, 0<N<10000.
2	6-10	L5	\$DYNAMIC	F T	FOR A STATIC ANALYSIS, SET \$DYNAMIC = F. FOR A DYNAMIC ANALYSIS, SET \$DYNAMIC = T.
2	11-15	I5	IMODE	0 1	FOR NO MODAL OUTPUT DATA FOR MODAL OUTPUT DATA.
2	16-20	I5	NDIMEN	0 1	DIMENSIONAL OUTPUT DATA. NONDIMENSIONAL OUTPUT.
2	21-25	I5	NTHMAX	8	SUMMED SOLUTION WILL BE PRINTED AT NTHMAX MERID- IANS, 0<NTHMAX<=36.
2	26-30	I5	IFREQ	2	SOLUTION WILL BE PRINTED AT THE FIRST STATION, EVERY SUBSEQUENT IFREQ STATION AND THE LAST STATION, 0<IFREQ<=KMAX.
2	31-35	I5	IPRINT	3	EVERY IPRINT CONVERGED SOLUTION WILL BE PRINT- ED.
2	36-40	I5	IBCINL	-1 0	IF THE SHELL HAS A POLE AT THE FIRST STATION. IF THE SHELL HAS NO POLE AT THE FIRST STATION.
2	41-45	I5	IBCFNL	-1 0	IF THE SHELL HAS A POLE AT THE LAST STATION. IF THE SHELL HAS NO POLE AT THE LAST STATION.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
2	46-50	I5	KMAX	35	NUMBER OF MERIDIONAL STATICS. NOTE: KMAX<201 FOR SATANS -I WITHOUT PLCTS AND KMAX<101 FOR SATANS-I WITH PLOTS OR FOR SATANS -II. SATANS-IIA IS UNLIMITED.
2	51-55	I5	MNMAX	7	NUMBER OF SERIES COEFFICIENTS USED TO DESCRIBE THE INITIAL CONDITIONS, PRESSURE AND THERMAL LOADS (AND INITIAL IMPERFECTIONS IF USING SATANS-II OR IIA). MNMAX<=MAXM.
2	56-60	I5	MAXM	7	MAX NUMBER OF HARMONICS IN THE SOLUTION, LIMITED TO 99.
2	61-65	I5	LSMAX	1 99 3000	FOR A LINEAR ANALYSIS. USE MANY LOAD STEPS FOR A NONLINEAR STATIC ANALYSIS. FOR A DYNAMIC ANALYSIS, LSMAX IS THE NUMBER OF TIME INCREMENTS, WHERE $LSMAX = T_{MAX}/\Delta T$.
2	66-70	I5	LCHMAX	2 0	THE NUMBER OF LOAD STEP SIZE REDUCTIONS IN A STATIC ANALYSIS, RECOMMENDED RANGE = 2-4. FOR A DYNAMIC ANALYSIS.
2	71-75	I5	ITRMAX	1 30	FOR A LINEAR ANALYSIS. THE NUMBER OF ITERATIONS AT A LOAD OR TIME STEP. FOR A NONLINEAR ANALYSIS, SUGGESTED RANGE = 10-30, UP TO 50 FOR SPECIAL CASES.
2	76-80	I5	IC	0 1	INITIAL CONDITIONS. SET TO 0 FOR A STATIC ANALYSIS, OR FOR A DYNAMIC ANALYSIS WHERE THE SHEL IS AT REST AT $T=0$. FOR A DYNAMIC ANALYSIS WITH INITIAL CONDITIONS.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
3	1-12	E12.3	NU	0.3	POISSON'S RATIO, ν .
3	12-24	E12.3	SIG0	1000.0 1.0	REFERENCE STRESS LEVEL, σ_0 . IF THE INPUT DATA IS DIMENSIONAL.
3	24-36	E12.3	ELAST	.3E8 1.0	REFERENCE MODULUS OF ELASTICITY, E_0 . IF THE INPUT DATA IS DIMENSIONAL.
3	37-48	E12.3	TKN	.4E-2 1.0	REFERENCE THICKNESS, h_0 . IF THE INPUT DATA IS DIMENSIONAL.
3	49-60	E12.3	CHAR	8.16 1.0	CHARACTERISTIC SHELL DIMENSION, a_0 . IF THE INPUT DATA IS DIMENSIONAL.
3	61-72	E12.3	TEEO	0.0 .996E-5	IF A STATIC ANALYSIS. REFERENCE TIME, T_0 .
<hr/>					
4	1-12	E12.3	DELCOAD	0.2 .1823E-6	FOR A STATIC ANALYSIS, DELCOAD IS THE LCOAD INCRE- MENT. IT REMAINS UN- CHANGED UNTIL THE SOLU- TION FAILS TO CONVERGE IN ITERMAX ITERATIONS, WHEN IT IS REDUCED BY A FACTOR OF FIVE. A MAXIMUM OF LCHMAX SUCH REDUCTIONS WILL OCCUR. FOR A DYNAMIC ANALYSIS, DELCOAD IS THE NONDIMEN- SIONAL TIME INCREMENT.
4	13-24	E12.3	EPS	0.01	THE CONVERGENCE CRITERION RECOMMENDED RANGE OF $0.01 < EPS < 0.001$.

CARD 4A IS ONLY INCLUDED FOR A SATANS-II OR SATANS-IIA RUN.

4A	1-5	I5	JUMP	1	FOR AN ANALYSIS USING SINGLE SERIES EXPANSIONS.
				2	FOR AN ANALYSIS USING DOUBLE SERIES EXPANSIONS.
4A	5-10	I5	MPERFS	0	AN ANALYSIS WITHOUT IM- PERFECTIONS.
				1	AN ANALYSIS WITH IMPEREC- TIONS. NOTE: IF JUMP=28 MPERFS MAY BE 0 OR 1. IF JUMP =1, MPERFS MUST BE 0. IF MPERFS=1, JUMP MUST BE 2.

CARD COLUMN FORMAT ITEM EXAMPLE MEANING

INCLUDE AS MANY CARDS 5 AS NECESSARY TO SPECIFY NTHMAX MERIDIANS. IF NTHMAX EQUALS 0, OMIT CARD 5.

5	1-72	6E12.3	10.0	A LIST OF CIRCUMFERENTIAL COORDINATES Θ , IN DEGREES AND TENTHS, WHERE THE SOLUTION PRINTOUT IS DESIRED. THE LIST MUST HAVE NTHMAX ENTRIES.
---	------	--------	------	--

IF IBCINL = -1, OMIT CARDS 6 THROUGH 14. IF IBCFNL = -1, OMIT CARDS 15 THROUGH 23. CARDS 6 THROUGH 23 DESCRIBE THE BOUNDARY CONDITIONS AT THE FIRST, AND THEN AT THE LAST STATION. THE BOUNDARY CONDITIONS EXIST ON THE TOTAL VARIABLES, NOT ON THE INDIVIDUAL HARMONICS. LOADINGS APPLIED THROUGH SPECIFICATION OF BOUNDARY CONDITIONS ARE TAKEN IN THE ZERO-ETH HARMONIC (N=0) ONLY, AS THE COLUMN MATRIX $\{f\}$ IS SET TO ZERO FOR HARMONICS GREATER THAN ZERO. THE BOUNDARY CONDITIONS ARE DIMENSIONAL. THE FORMAT OF CARDS 6 THROUGH 23 IS 4E16.8.

CARD 6,15 CARD 7,16 CARD 8,17 CARD 9,18

$$\begin{bmatrix} n(1,1) \\ n(2,1) \\ n(3,1) \\ n(4,1) \end{bmatrix} \begin{bmatrix} n(1,2) \\ n(2,2) \\ n(3,2) \\ n(4,2) \end{bmatrix} \begin{bmatrix} n(1,3) \\ n(2,3) \\ n(3,3) \\ n(4,3) \end{bmatrix} \begin{bmatrix} n(1,4) \\ n(2,4) \\ n(3,4) \\ n(4,4) \end{bmatrix} \begin{bmatrix} N \\ N \\ N \\ N \end{bmatrix} +$$

$$\begin{bmatrix} \Lambda(1,1) \\ \Lambda(2,1) \\ \Lambda(3,1) \\ \Lambda(4,1) \end{bmatrix} \begin{bmatrix} \Lambda(1,2) \\ \Lambda(2,2) \\ \Lambda(3,2) \\ \Lambda(4,2) \end{bmatrix} \begin{bmatrix} \Lambda(1,3) \\ \Lambda(2,3) \\ \Lambda(3,3) \\ \Lambda(4,3) \end{bmatrix} \begin{bmatrix} \Lambda(1,4) \\ \Lambda(2,4) \\ \Lambda(3,4) \\ \Lambda(4,4) \end{bmatrix} \begin{bmatrix} U \\ V \\ W \\ M \end{bmatrix} = \begin{bmatrix} f(1) \\ f(2) \\ f(3) \\ f(4) \end{bmatrix}$$

CARD 24 IS:

1. INCLUDED FOR A SATANS-I STATIC ANALYSIS.
2. INCLUDED BUT BLANK FOR A SATANS-I DYNAMIC ANALYSIS.
3. OMITTED FOR A SATANS-II ANALYSIS.
4. INCLUDED BLANK FOR DYNAMIC USED FOR STATIC SATANS-IIA ANALYSES.

CARD COLUMN FORMAT ITEM EXAMPLE MEANING

24	1-2	L2	\$PLOTS	F	INDICATES PLOTS ARE NOT DESIRED.
				T	INDICATES PLOTS ARE DESIRED.
24	3-4	L2	\$MODAL	F	INDICATES PLOTS ARE FOR SUMMED SOLUTIONS ONLY.
				T	INDICATES PLOTS ARE FOR MODAL SOLUTIONS ONLY.

FOR THE REMAINDER OF CARD 24 ENTRIES, 0 INDICATES THAT NO PLOTS ARE DESIRED FOR THE PARTICULAR ITEM, AND 1 INDICATES THAT THEY ARE DESIRED. ALL GRAPHS ARE PLOTTED AS THE INDICATED ITEM VERSUS THE STATION NUMBER. IF A COMPLETE PLOT IS DESIRED, INSUTE IFREQ = 1.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	5-6	I2	IRADII	1	PLCT THE RADII AS COMPUTED BY SUBROUTINE GEOM.
24	7-8	I2	IGAMMA	1	PLCT P'/P AS COMPUTED BY SUBROUTINE GEOM.
24	9-10	I2	IOMEGS	1	PLCT ω_s AS COMPUTED BY SUBROUTINE GEOM.
24	11-12	I2	IOMEGT	1	PLCT ω_θ AS COMPUTED BY SUBROUTINE GEOM.
24	13-14	I2	IDECMS	1	PLCT ω'_s AS COMPUTED BY SUBROUTINE GEOM.
24	15-16	I2	IBSTIF	1	PLCT THE STIFFNESS D AS COMPUTED BY SUBROUTINE BDB.
24	17-18	I2	IDSTIF	1	PLOT THE STIFFNESS D AS COMPUTED BY THE SUBROUTINE BDB.
24	19-20	I2	IBBSTF	1	PLCT THE STIFFNESS db/ds AS COMPUTED BY SUBROUTINE BDB.
24	21-22	I2	IDDSTF	1	PLCT THE STIFFNESS dd/ds AS COMPUTED BY SUBROUTINE BDB.
24	23-24	I2	IPR	1	PLOT THE NORMAL COMPONENT OF THE PRESSURE LOAD.
24	25-26	I2	IPS	1	PLOT THE MERIDIONAL COMPONENT OF THE PRESSURE LOAD.
24	27-28	I2	IPT	1	PLCT THE CIRCUMFERENTIAL COMPONENT OF THE PRESSURE LOAD.
24	29-30	I2	ITT	1	PLCT THE THERMAL LOAD.
24	31-32	I2	IMT	1	PLOT THE THERMAL MOMENT.
24	33-34	I2	IDTT	1	PLCT d/ds OF THE THERMAL LOAD.
24	35-36	I2	IDMT	1	PLOT d/ds OF THE THERMAL MOMENT.
24	37-38	I2	INS	1	PLOT THE MERIDIONAL MEMBRANE FORCE DISTRIBUTION.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	39-40	I2	INTH	1	PLCT THE CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	41-42	I2	INSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	43-44	I2	IQS	1	PLCT THE TRANSVERSE FORCE DISTRIBUTION.
24	45-46	I2	IMS	1	PLCT THE MERIDIONAL MOMENT DISTRIBUTION.
24	47-48	I2	IMTH	1	PLCT THE CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	49-50	I2	IMSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	51-52	I2	IU	1	PLCT THE MERIDIONAL DISPLACEMENT DISTRIBUTION.
24	53-54	I2	IV	1	PLCT THE CIRCUMFERENTIAL DISPLACEMENT DISTRIBUTION.
24	55-56	I2	IW	1	PLCT THE NORMAL DISPLACEMENT DISTRIBUTION.
24	57-58	I2	IPHIS	1	PLCT THE MERIDIONAL ROTATION DISTRIBUTION.
24	59-60	I2	IPHIT	1	PLCT THE CIRCUMFERENTIAL ROTATION DISTRIBUTION.
24	61-62	I2	IPHI	1	PLCT THE MERIDIO-CIRCUMFERENTIAL ROTATION DISTRIBUTION.

INCERT IMPERFECTION DATA HERE FOR A SATANS-II OR SATANS-IIA ANALYSIS WITH IMPERFECTIONS. INSURE FORMAT OF THE IMPERFECTION DATA IS COMPATIBLE WITH THAT SPECIFIED IN THE USER-WRITTEN SUBROUTINE IMPERF.

25	1-2	I2	IRNAGN	0	INDICATES THIS IS THE ONLY RUN.
				1	INDICATES ANOTHER RUN IS TO BE MADE. ADD ANOTHER COMPLETE SET OF DATA CARDS AFTER THIS CARD IS IRNAGN= 1.

APPENDIX D

LISTING OF NEW POLE ROUTINE FOR SATANS-IIA

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE FCRCE SUBROUTINE

CCMMCN /IEL5/IBCINL,IBCFNL

```

C      IN FCRCE
10    IF(K.NE.2.OR.(K.EQ.2.AND.IBCINL.GE.0)) GO TO 501
      DC 502 II=1,4
      SUMX=0.
      DC 503 L=1,4
      SUMX=SUMX+DL(II,L,M)*GEE(L)
902   X(II,IK1)=SUMX
901   CCNTINUE
      DC 11 I=1,4

```

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE PMATRX SUBROUTINE

```

C      IN PMATRX
      CALL EFG(2,MN)
      CALL ABC
      CALL MATINV(A,4,G1,0,DETERM,IPIVCT,INDEX,4,ISCALE)
      DC 501 II=1,4
      DC 501 JJ=1,4
      CL(II,JJ,MN)=0.
      CG(II,JJ,MN)=0.
      CF(II,JJ,MN)=0.
      IF(MN.GT.1) GO TO 12
      IF(MN.GT.0) GO TO 13
901

```



```

NC=MN
  CL(1,1,MN)=1.
  CL(1,2,MN)=1.
  CL(1,3,MN)=-3.
  CL(1,4,MN)=-3.
  CG(3,3,MN)=4.
  CG(4,4,MN)=4.
  CF(3,3,MN)=-1.
  CF(4,4,MN)=-1.
  GC TO 9C2
13 IF I=MN
  CL(1,1,MN)=-3.
  CL(1,2,MN)=1.
  CL(1,3,MN)=1.
  IF(A(M1).LT.0) DL(2,2,MN)=-1
  CL(3,3,MN)=1.
  CL(4,4,MN)=1.
  CG(1,1,MN)=4.
  CF(1,1,MN)=-1.
  GC TO 9C2
12 M2=MN
  CL(1,1,MN)=1.
  CL(1,2,MN)=1.
  CL(1,3,MN)=1.
  CL(1,4,MN)=-3.
  CG(4,4,MN)=4.
  CF(4,4,MN)=-1.
  CC CONTINUE
  CC SC3 II=1,4
  CC SC3 JJ=1,4
  TTF=0.
  CC SC4 L=1,4
  TTF=TP+DF(II,L,MN)*A(L,JJ)
9C4 CL0(II,JJ)=TTP
9C5 CC SC5 II=1,4
  CC SC5 JJ=1,4
  TTF=0.
  TTF=0.
  CC 906 L=1,4
  TTF=TP+CL0(II,L)*C(L,JJ)
9C6 TTF=TP+CLC(II,L)*BEE(L,JJ)
  CL1(II,JJ)=DL(II,JJ,MN)-TTP
9C5 CL2(II,JJ)=DG(II,JJ,MN)-TTC
  CALL MATINV(CLI,4,G1,0,DETERM,IPIVOT,INDEX,4,ISCALE)
  CC SC7 II=1,4
  CC SC7 JJ=1,4
  TTF=0.
  TTF=0.

```



```

      CC SC8 L=1,4
      TTP=CL1(I1,I1,L)*CL0(L,JJ)
      TTQ=TTQ+CL1(I1,I1,L)*CL2(L,JJ)
      SC8 LL(I1,JJ,MN)=-TTP
      SC7 P(I1,J,IJ)=TTQ
      SC CC TC 11
      SC P3=MN

```


APPENDIX E

LISTING OF CARDS FOR \bar{V} AND \bar{V}_{MAX}

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE DYNAMIC SUBROUTINE IF NEEDED

```

C      STATEMENTS FOR MAIN TO CALCULATE VBAR
185  DENCN=.125*CMXI(KMAX)*R(KMAX)**4
CC 186  N=1,MAXM
      CNLN=0.
      NM=(M-1)*KMAX2
CC 184  K=2,KL
      KT=K+1+MM
184  CNLN=CNLN+Z(3,KT)*R(K)
      CNLN=CNLN*DEL#SOE
186  VBAR(M)=CNLN/DENCN
      ITTEST=ITTEST+1
      IF(ITTEST.NE.10) GC TO 963
      ITTEST=C
      WRITE(6,183)(LSTEP,VBAR(M),M=1,MAXM)
183  FORMAT(/5X,'VBAR AT TIME STEP ',I4,' FOR EACH MODE IS',5E16.4)
963  CC 187  N=1,MAXM
      IF(LSTEP.EQ.1) AVB(M)=0.
187  IF(ABS(VBAR(M)).GT.AVB(M)) AVB(M)=ABS(VBAR(M))

```


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